

Appendix–A: Regression Modeling of Experimental Data

I) The Generalized Random Variable Linear Regression Model:

The model equation can be written as:

$$\hat{Y}_i = \beta_0 + \beta_1 x_i + \hat{\varepsilon}_i \quad \text{----- (A1)}$$

Where:

$$\hat{\varepsilon}_i \equiv N[0, \sigma^2]$$

I-1) Confidence bound on $\hat{\beta}_0$ (100(1- α) % interval) is $\hat{\beta}_0 - \theta < \beta_0 \leq \hat{\beta}_0 + \theta$

with $\theta \equiv \left(t_{\alpha/2, (n-2)} \right) S_e \left(\hat{\beta}_0 \right)$.

With the standard error of the intercept as:

$$S_e \left(\hat{\beta}_0 \right) = \sqrt{MS_{res} \left(\frac{1}{n} + \frac{\bar{X}^2}{S_{XX}} \right)} \quad \text{----- (A2)}$$

Where:

$$S_{XX} = \sum_{i=1}^n (x_i - \bar{X})^2$$

$$MS_{res} = \text{Residual Mean Square} = \frac{SS_{res}}{n-2} \equiv \hat{\sigma}^2$$

$$SS_{res} = SS_{Total} - \hat{\beta}_1 S_{XY}$$

$$\hat{\beta}_1 = \frac{S_{XY}}{S_{XX}} = \frac{\sum_{i=1}^n Y_i (X_i - \bar{X})}{\sum_{i=1}^n (X_i - \bar{X})^2} \text{----- (A3)}$$

$$SS_{Total} = \sum_{i=1}^n (Y_i - \bar{Y})^2 \text{----- (A4)}$$

$$\bar{X} = \frac{\sum_{i=1}^n X_i}{n} \text{ and } \bar{Y} = \frac{\sum_{i=1}^n Y_i}{n} \text{----- (A5)}$$

$$\hat{\beta}_0 = \bar{Y} - \hat{\beta}_1 \bar{X}$$

n = Number of observations

$$\left(t_{\alpha/2, (n-2)} \right) = \text{“t” statistic}$$

I-2) Confidence bound on $\hat{\beta}_1$ (100(1- α) % Estimate) is $\hat{\beta}_1 - \theta_1 < \beta_1 \leq \hat{\beta}_1 + \theta_1$

$$\text{With } \theta_1 \equiv \left(t_{\alpha/2, (n-2)} \right) S_e \left(\hat{\beta}_1 \right)$$

Where the standard error of the intercept is:

$$S_e \left(\hat{\beta}_1 \right) = \sqrt{\frac{MS_{res}}{SS_{XX}}} \text{----- (A6)}$$

I-3) Interval Estimate of Expectation Value:

The estimate of the expectation value of $Y_i \left(\mu_{Y_i/X_i}^{\wedge} \right)$ can be written as:

$$\hat{E} \left(Y_i / X_i \right) = \mu_{Y_i/X_i}^{\wedge} = \hat{\beta}_0 + \hat{\beta}_1 X_i \quad \text{----- (A7)}$$

The interval bounds for this parameter are:

$$\left[\mu_{Y_i/X_i}^{\wedge} - \theta_2 \right] < E \left(Y_i / X_i \right) \leq \left[\mu_{Y_i/X_i}^{\wedge} + \theta_2 \right] \quad \text{----- (A8)}$$

$$\text{With } \theta_2 \equiv \left(t_{\alpha/2, (n-2)} \right) \sqrt{MS_{res} \left[\frac{1}{n} + \frac{(X_i - \bar{X})^2}{S_{XX}} \right]}$$

I-4) New 'Prediction' Value:

The expressions are:

$$\left[\hat{Y}_i - \theta_3 \right] < Y_i \leq \left[\hat{Y}_i + \theta_3 \right] \quad \text{----- (A9)}$$

$$\text{With } \theta_3 \equiv \left(t_{\alpha/2, (n-2)} \right) \sqrt{MS_{res} \left[1 + \frac{1}{n} + \frac{(X_i - \bar{X})^2}{S_{XX}} \right]}$$

I-5) Coefficient of determination for generalized regression equation is:

$$R^2 = 1 - \frac{SS_{res}}{SS_{Total}} \quad \text{----- (A10)}$$

II) Constrained Random Variable Linear Regression Model:

The model equation can be written as:

$$\hat{Y}_i = \beta_2 x_i + \varepsilon_i \quad \text{----- (A}_{11}\text{)}$$

Where:

$$\varepsilon_i \equiv N[0, \sigma^2] \text{ with } \hat{\sigma}^2 = MS_{res} \equiv \frac{\sum_{i=1}^n (Y_i - \hat{Y}_i)^2}{n-1}$$

$$\hat{\beta}_2 = \frac{\sum_{i=1}^n X_i Y_i}{\sum_{i=1}^n X_i^2} \quad \text{----- (A}_{12}\text{)}$$

II-1) Confidence bound on $\hat{\beta}_2$ (100(1- α) % interval) is $\hat{\beta}_2 - \theta_4 < \beta_2 \leq \hat{\beta}_2 + \theta_4$

with $\theta_4 \equiv \left(t_{\alpha/2, (n-2)} \right) S_e \left(\hat{\beta}_2 \right)$.

Where the standard error of the intercept is:

$$S_e \left(\hat{\beta}_2 \right) = \sqrt{\frac{MS_{res}}{\sum_{i=1}^n X_i^2}} \quad \text{----- (A}_{13}\text{)}$$

II-2) Interval Estimate of Expectation Value:

The estimate of the expectation value of $Y_i \left(\mu_{Y_i/x_i} \right)$ can be written as:

$$\hat{E}\left(\frac{Y_i}{X_i}\right) = \mu_{Y_i/X_i}^{\hat{}} = \hat{\beta}_2 X_i \quad \text{----- (A14)}$$

The interval bounds for this parameter are

$$\left[\mu_{Y_i/X_i}^{\hat{}} - \theta_5 \right] < E\left(\frac{Y_i}{X_i}\right) \leq \left[\mu_{Y_i/X_i}^{\hat{}} + \theta_5 \right] \quad \text{----- (A15)}$$

$$\text{With } \theta_5 \equiv \left(t_{\alpha/2, (n-1)} \right) \sqrt{\frac{X_i^2 (MS_{res})}{\sum_{i=1}^n X_i^2}}$$

II-3) New “Prediction” Value:

The expressions are:

$$\left[\hat{Y}_i - \theta_6 \right] < Y_i \leq \left[\hat{Y}_i + \theta_6 \right] \quad \text{----- (A16)}$$

$$\text{With } \theta_6 \equiv \left(t_{\alpha/2, (n-1)} \right) \sqrt{MS_{res} \left[1 + \frac{X_i^2}{\sum_i X_i^2} \right]}$$

II-4) Coefficient of determination for constrained regression equation is:

$$R_0^2 = \frac{\sum_{i=1}^n \hat{Y}_i^2}{\sum_{i=1}^n Y_i^2} \quad \text{----- (A17)}$$

Appendix–B: Formulations of Van’t Hoff Relation

Two different derivations of the form of the “Van’t Hoff” expression are presented as below:

Derivation–1:

The Clausius – Clapeyron equation is given by:

$$\frac{d(\ln P)}{dT} = \frac{\Delta H^{l \rightarrow v}}{RT^2} \quad \text{----- (B}_1\text{)}$$

The above equation describes a vapor – condensed phase equilibrium of the form:



On the other hand (in our case), the reaction is considering of the form:



Assuming α_{solid} and αH_2 to be in standard state (pure substance),

$$\Delta G_T = \Delta G_T^0 + RT \ln K = \Delta G_T^0 + RT \ln \frac{a_{\alpha H_2}}{a_{\alpha} a_{H_2}} \quad \text{----- (B}_4\text{)}$$

Since, $a_{\alpha H_2} = a_{\alpha} = 1$, and $a_{H_2} = \frac{P_{H_2}}{P_{H_2}^0}$.

Therefore, Eqn. (B₄) can write;

$$\therefore \Delta G_T = \Delta G_T^0 + RT \ln \left(\frac{1}{\frac{P_{H_2}}{P_{H_2}^0}} \right) \text{----- (B5)}$$

Now, at equilibrium at any temperature, $\Delta G_T \equiv 0$. This implies:

$$-\ln \left(\frac{P_{H_2}}{P_{H_2}^0} \right) = -\frac{\Delta G_T^0}{RT} \text{----- (B6)}$$

$$\text{But, } \Delta G_T^0 = \Delta H_T^0 - T\Delta S_T^0$$

$$\therefore \ln \left(\frac{P_{H_2}}{P_{H_2}^0} \right) = \frac{\Delta H_T^0}{RT} - \frac{\Delta S_T^0}{R} \text{----- (B7)}$$

If $\Delta H_T^0 \neq \phi(T)$ and $\Delta S_T^0 \neq \phi(T)$, then Eqn. (B7) can write:

$$\ln \left(\frac{P_{H_2}}{P_{H_2}^0} \right) = \left(\frac{\Delta H^0}{R} \right) \frac{1}{T} - \frac{\Delta S^0}{R} \text{----- (B8)}$$

$$\ln \left(\frac{P_{H_2}}{P_{H_2}^0} \right) = \frac{\alpha_1}{T} + \alpha_2 \text{----- (B9)}$$

$$\text{With, } \alpha_1 = \frac{\Delta H^0}{R} \text{ and } \alpha_2 = -\frac{\Delta S^0}{R}$$

If one now applies Eqns. (B7) or (B8) to two temperatures T_1 and T_2 , we can write,

$$\ln\left(\frac{(P_{H_2})_{T_2}}{P_{H_2}^0}\right) - \ln\left(\frac{(P_{H_2})_{T_1}}{P_{H_2}^0}\right) = \frac{\Delta H^0}{R} \left[\frac{1}{T_2} - \frac{1}{T_1} \right] \quad \text{----- (B10)}$$

$$\ln\left(\frac{(P_{H_2})_{T_2}}{(P_{H_1})_{T_1}}\right) = \frac{\Delta H^0}{R} \left[\frac{1}{T_2} - \frac{1}{T_1} \right] \quad \text{----- (B11)}$$

At this point, it is to be noted that in the chemical equilibrium considered for Eq. (B7) or (B8), the vapor (gaseous) phase is placed on the left hand side of Eq. (B3). If in the condensation reaction considered by Eq. (B2), the vapor phase is placed on the left hand side as:

$$\alpha_{\text{vapor}} \Leftrightarrow \alpha_{\text{liquid}} \quad \text{----- (B12)}$$

Then, Clausius – Clapeyron equation will read:

$$\left(\frac{dP}{dT}\right)_{eq} = \frac{\Delta H^{v \rightarrow l}}{T(V^l - V^v)} \cong -\frac{\Delta H^{v \rightarrow l}}{TV^v} \quad \text{----- (B13)}$$

$$\text{or } \left(\frac{dP}{P}\right)_{eq} = -\frac{\Delta H^{v \rightarrow l}}{RT^2} \quad \text{----- (B14)}$$

On integration of above equation one obtains:

$$\ln P = \frac{\Delta H^{v \rightarrow l}}{RT} + \alpha_2 \quad \text{----- (B15)}$$

$$\text{or } \ln P = \frac{\alpha_1}{T} + \alpha_2 \quad \text{----- (B16)}$$

or between station temperatures T_1 and T_2 , we can write:

$$\ln \frac{P_2}{P_1} = \frac{\Delta H^{v \rightarrow l}}{R} \left[\frac{1}{T_2} - \frac{1}{T_1} \right] \text{----- (B17)}$$

Derivation-2:

The Van't Hoff relationship can also deduce using the following two identities,

$$\left[\frac{\partial \left(\frac{\Delta G^0}{T} \right)}{\partial T} \right]_P = -\frac{\Delta H^0}{T^2} \text{----- (B18)}$$

$$\text{and } \left[\frac{\partial (\Delta G^0)}{\partial T} \right]_P = -\Delta S^0 \text{----- (B19)}$$

Now, from Eqns. (B3) and (B4), we have:

$$\Delta G = \Delta G^0 + RT \ln K_p \text{----- (B20)}$$

Or at equilibrium:

$$\Delta G = 0 = \Delta G^0 + RT \ln K_p \text{----- (B21)}$$

$$\text{or } \Delta G^0 = -RT \ln K_p \text{----- (B22)}$$

Plugging Eq. (B22) into Eqns. (B18) and (B19), we obtain;

$$\frac{\partial (\ln K_p)}{\partial T} = \frac{\Delta H^0}{T^2} \text{----- (B23)}$$

$$\text{and } T \frac{\partial(\ln K_p)}{\partial T} + \ln K_p = \frac{\Delta S^0}{R} \quad \text{----- (B}_{24}\text{)}$$

Plugging Eq. (C₂₄) into Eq. (C₂₃), we obtain:

$$\ln K_p = -\frac{\Delta H^0}{RT} + \frac{\Delta S^0}{R} \quad \text{----- (B}_{25}\text{)}$$

$$\text{Now, } K_p = \frac{1}{\frac{P_{H_2}}{(P_{H_2})^{\text{Ref}}}} \quad \text{----- (B}_{26}\text{)}$$

$$\ln \frac{P_{H_2}}{(P_{H_2})^{\text{Ref}}} = \frac{\Delta H^0}{RT} - \frac{\Delta S^0}{R} \quad \text{----- (B}_{27}\text{)}$$

Note that, Eq. (B₂₇) is of the form:

$$\ln \left(\frac{P_{H_2}}{P_{H_2}^{\text{Ref}}} \right) = \frac{\alpha_1}{T} + \alpha_2 \quad \text{----- (B}_{28}\text{)}$$