Appendix A

Calibration of Instruments and Connecting Pipes

A.1 Pressure Transmitter Used to Measure Test Chamber Pressure

Endress+Hauser make pressure transmitter of model no. Cerabar SPMC71: A50CB20109C was mounted on the top of the test section to measure the air pressure. The pressure transmitter was factory calibrated and calibration results are shown in Table A.1.

% of span	Pressure input (bar)	Expected (Volts dc)	Actual (Volts dc)
100	10.0	5.0000	5.0005
75	7.5	4.0000	4.0007
50	5.0	3.0000	3.0001
25	2.5	2.0000	2.0003
0	0.0	1.0000	1.0001

Table A.1: Calibration data from pressure transmitter located at test section

A.2 Pressure Transmitter Used to Measure Phase Separators Pressure

Two Honeywell ST 3000 pressure transmitters of model no. STG140 were used in the experiment to measure the pressure of 1PH, and 2PH. Each pressure transducer was factory calibrated. Calibration results of both the pressure transmitters are shown in Table A.2 and Table A.3. The manufacturer calibrated the pressure transmitters with air at 26^oC temperature and with 69% humidity.

% of span	Pressure input	Expected	Actual
	(bar)	(Volts dc)	(Volts dc)
100	10.0	5.0000	4.9998
75	7.5	4.0000	4.0001
50	5.0	3.0000	3.0003
0	2.5 0.0	2.0000	2.0001 0.9997

Table A.2:Calibration data from pressure transmitter located at 1PH

Table A. 3 : Calibration data from pressure transmitter located at 2PH

% of span	Pressure input (bar)	Expected (Volts dc)	Actual (Volts dc)
100	10.0	5 0000	5 0001
75	7.5	4.0000	4.0000
50	5.0	3.0000	2.9997
25	2.5	2.0000	1.9997
0	0.0	1.0000	0.9992
1			

A.3 Water Mass Flow Meter

A mass flow meter operating on coriolis measuring principle was used in experiment to measure the water flow rate discharging from phase separator. The mass flow meter was installed at the downstream of the 1PH. The mass flow meter was factory calibrated with water. Calibration results of the mass flow meters are shown in Table A.4.

Flow (%)	Flow (kg/hr)	Duration (s)	Target mass (kg)	Measured mass (kg)	Deviation of reading (%)	Output (mA)
20.0	720.4	30.0	6.009	6.0116	0.028	7.20
34.7	1249.6	143.8	49.930	49.928	-0.003	9.55
50.0	1799.6	99.8	49.898	49.894	-0.007	12.00
74.3	2673.7	67.4	50.067	50.066	-0.002	15.88
100.1	3602.5	50.0	50.037	50.038	0.000	20.01

Table A. 4 : Calibration data from a mass flow meter located at downstream of 1PH

A.4 Calibration of Liquid Height

The objective was to calibrate the measured liquid height seen through the recording camera with respect to the actual height of the liquid in the glass tube. The calibration was done over the range of 2.25 mm to 59.00 mm of liquid height in the liquid level indicator as shown in Figure A.1.

A.5 Calibration of Connecting Pipes

The objective was to calibrate the connecting pipe for varying ΔP with fixed opening of the control valve located at the downstream of the branch. At each ΔP of 0.25, 0.50, 0.75, 1.00, 2.00, 3.00, 4.00 and 4.50 bar the variation in Fr_L within the operating range of ΔP is shown in Figure A.2.



Figure A. 1 : Calibration of liquid height



Figure A. 2 : Calibration of connecting pipes for varying ΔP



Figure A.2 : Calibration of connecting pipes for varying ΔP (cont.)

Appendix B

Estimation of Uncertainty

This appendix provides the measure of the reliability of the experimental results.

B.1 Experimental Uncertainty in the Data

Kline and McClintock (1953) and Moffat (1988) method was followed for estimation of experimental uncertainty for independent and dependent variables. All the uncertainties estimated are at "odds" of 20 to 1. The uncertainties include the accuracy of the calibrating device, the error in fitting an equation (for computer data reduction) to the calibration data, discrimination uncertainties in the measuring instruments and unsteadiness in the process.

If the result R is the function of an independent variable v_1 , v_2 ,... v_n , each of which is normally distributed, then the relation between the interval for the variables wv_1 , and the interval for the result wR, which gives the same odds for each of the variable and for the result is

$$wR = \pm \left[\left(\frac{\partial R}{\partial v_1} w v_1 \right)^2 + \left(\frac{\partial R}{\partial v_2} w v_2 \right)^2 + \dots + \left(\frac{\partial R}{\partial v_n} w v_n \right)^2 \right]^{1/2}$$
(B.1)

The relative uncertainty in the result is represented by:

$$\frac{\mathrm{wR}}{\mathrm{R}} = \pm \left[\left(\frac{\partial \mathrm{R}}{\partial \mathrm{v}_1} \frac{\mathrm{wv}_1}{\mathrm{R}} \right)^2 + \left(\frac{\partial \mathrm{R}}{\partial \mathrm{v}_2} \frac{\mathrm{wv}_2}{\mathrm{R}} \right)^2 + \dots + \left(\frac{\partial \mathrm{R}}{\partial \mathrm{v}_n} \frac{\mathrm{wv}_n}{\mathrm{R}} \right)^2 \right]^{1/2}$$
(B.2)

B.2 Uncertainty in P_{TC}

The instrument uncertainty of the pressure transmitter used to measure the air pressure in the test section and the uncertainty due to the fluctuation in the process was calculated as follows;

$$\frac{wP_{TC}}{P_{TC}} = \pm \sqrt{\left(\frac{wP_{TC,T}}{P_{TC}}\right)^2 + \left(\frac{wP_{TC,P}}{P_{TC}}\right)^2}$$
(B.3)

B.3 Uncertainty in P_{PH}

The instrument uncertainty of the pressure transmitter used to measure the pressure of the phase separators and the uncertainty due to fluctuation in the process was calculated as below;

$$\frac{wP_{PH}}{P_{PH}} = \pm \sqrt{\left(\frac{wP_{PH,T}}{P_{PH}}\right)^2 + \left(\frac{wP_{PH,P}}{P_{PH}}\right)^2}$$
(B.4)

B.4 Uncertainty in ΔP

Applying equation (B.2) to equation (B.5), the relative uncertainty for the pressure drop across the branches is calculated using equation (B.6).

$$\Delta P = (P_{TC} - P_{PH})$$
(B.5)

$$\frac{\partial \Delta P}{\partial P_{TC}} = (1)$$

$$\frac{\partial \Delta P}{\partial P_{PH}} = (-1)$$

$$w\Delta P = \pm \left[\left(\frac{\partial \Delta P}{\partial P_{TC}} w P_{TC} \right)^2 + \left(\frac{\partial \Delta P}{\partial P_{PH}} w P_{PH} \right)^2 \right]^{1/2}$$

$$\frac{w\Delta P}{\Delta P} = \pm \left[\left(\frac{\partial \Delta P}{\partial P_{TC}} \frac{w P_{TC}}{\Delta P} \right)^2 + \left(\frac{\partial \Delta P}{\partial P_{PH}} \frac{w P_{PH}}{\Delta P} \right)^2 \right]^{1/2}$$

$$\frac{w\Delta P}{\Delta P} = \pm \left[\left(1 \frac{1}{(P_{TC} - P_{PH})} w P_{TC} \right)^2 + \left(-1 \frac{1}{(P_{TC} - P_{PH})} w P_{PH} \right)^2 \right]^{1/2}$$
(B.6)

The uncertainty interval quoted by the manufacturer is ± 0.015 bar for the P_{TC} and ± 0.019 bar for the P_{PH}.

B.5 Uncertainty in ρ_G

Applying equation (B.2) to ideal gas law equation (B.7), the relative uncertainty for the density of air within the test section was calculated using equation (B.8).

$$\rho_{G} = \frac{P_{TC,abs}}{R_{G}T_{G}}$$
(B.7)

$$\frac{\partial \rho_{G}}{\partial P_{TC,abs}} = \left(\frac{1}{R_{G}T_{G}}\right)$$

$$\frac{\partial \rho_{G}}{\partial R_{G}} = \left(\frac{-P_{TC,abs}}{R_{G}^{2}T_{G}}\right)$$

$$\frac{\partial \rho_{G}}{\partial T_{G}} = \left(\frac{-P_{TC,abs}}{R_{G}T_{G}^{2}}\right)$$

$$w\rho_{G} = \pm \left[\left(\frac{\partial \rho_{G}}{\partial P_{TC,abs}} wP_{TC,abs}\right)^{2} + \left(\frac{\partial \rho_{G}}{\partial R_{G}} wR_{G}\right)^{2} + \left(\frac{\partial \rho_{G}}{\partial T_{G}} wT_{G}\right)^{2}\right]^{\frac{1}{2}}$$

$$\frac{w\rho_{G}}{\rho_{G}} = \pm \left[\left(\frac{\partial \rho_{G}}{\partial P_{TC,abs}} \frac{wP_{TC,abs}}{\rho_{G}}\right)^{2} + \left(\frac{\partial \rho_{G}}{\partial R_{G}} \frac{wR_{G}}{\rho_{G}}\right)^{2} + \left(\frac{\partial \rho_{G}}{\partial T_{G}} \frac{wT_{G}}{\rho_{G}}\right)^{2}\right]^{\frac{1}{2}}$$

$$\frac{w\rho_{G}}{\rho_{G}} = \pm \left[\left(\frac{1}{R_{G}T_{G}} \frac{R_{G}T_{G}}{P_{TC,abs}} wP_{TC,abs}\right)^{2} + \left(\frac{-P_{TC,abs}}{R_{G}^{2}T_{G}} \frac{R_{G}T_{G}}{P_{TC,abs}} wR_{G}\right)^{2} + \left(\frac{-P_{TC,abs}}{R_{G}^{2}T_{G}} \frac{R_{G}T_{G}}{P_{TC,abs}} wR_{G}\right)^{2}$$

$$+ \left(\frac{-P_{TC,abs}}{R_{G}T_{G}^{2}} \frac{R_{G}T_{G}}{P_{TC,abs}} wT_{G}\right)^{2} + \left(-\frac{wT_{G}}{T_{G}}\right)^{2}\right]^{\frac{1}{2}}$$

The error in the characteristic gas constant is assumed negligible, $wR_G \simeq 0$.

$$\frac{w\rho_{G}}{\rho_{G}} = \pm \left[\left(\frac{wP_{TC,abs}}{P_{TC,abs}} \right)^{2} + \left(-\frac{wT_{G}}{T_{G}} \right)^{2} \right]^{1/2}$$
(B.8)

The uncertainty interval quoted by manufacturer for T_G is ± 0.5 $^0C.$

B.6 Uncertainty in $\Delta \rho$

Applying equation (B.2) to the equation (B.9), the relative uncertainty for the $\Delta \rho$ was calculated using equation (B.10).

$$\Delta \rho = \rho_{\rm L} - \rho_{\rm G} \tag{B.9}$$

$$\frac{w\Delta \rho}{\Delta \rho} = \pm \left[\left(\frac{w\rho_{\rm L}}{\Delta \rho} \right)^2 + \left(- \frac{w\rho_{\rm G}}{\Delta \rho} \right)^2 \right]^{1/2}$$

$$w\rho_{\rm L} = 0 \text{ (negligible)}$$

$$\frac{w\Delta \rho}{\Delta \rho} = \pm \left[\left(- \frac{w\rho_{\rm G}}{\Delta \rho} \right)^2 \right]^{1/2} \tag{B.10}$$

B.7 Uncertainty in m_L

The uncertainty quoted by the manufacturer for \dot{m}_L is given below;

% Error in flow =
$$\pm \left(0.25 + \left(\frac{6 - \dot{m}_{L}}{14} \right) + \left(\frac{9}{1000 \times \dot{m}_{L}} \right) \right)$$
 (B.11)

for 2.5 $\,<\dot{m}_L<6$

% Error in flow =
$$\pm \left(0.05 + \left(\frac{12 - \dot{m}_L}{30} \right) + \left(\frac{9}{1000 \times \dot{m}_L} \right) \right)$$
 (B.12)

for $6 \leq ~\dot{m}_L < 12$

% Error in flow =
$$\pm \left(0.05 + \left(\frac{9}{1000 \times \dot{m}_{L}} \right) \right)$$
 (B.13)

for $\dot{m}_L \ge 12$

B.8 Uncertainty in h_{OGE}

The uncertainty in measuring h_{OGE} was \pm 0.25 mm due to minimum visualization accuracy of the human eye while reading the flat rule scale.

B.9 Uncertainty in Fr_L

Applying equation (B.2) to equation (B.14), the relative uncertainty for the Froude Number is calculated using equation (B.15).

$$\begin{aligned} \mathrm{Fr}_{\mathrm{L}} &= \frac{4 \, \dot{\mathrm{m}}_{\mathrm{L}}}{\pi \sqrt{\mathrm{g}} \, \mathrm{d}^{5} \, \rho_{\mathrm{L}} \left(\rho_{\mathrm{L}} - \rho_{\mathrm{G}} \right)} \end{aligned} \tag{B.14} \\ &\frac{\partial \mathrm{Fr}_{\mathrm{L}}}{\partial \dot{\mathrm{m}}_{\mathrm{L}}} = \frac{4}{\pi \sqrt{\mathrm{g}} \, \mathrm{d}^{5} \, \rho_{\mathrm{L}} \left(\rho_{\mathrm{L}} - \rho_{\mathrm{G}} \right)} \\ &\frac{\partial \mathrm{Fr}_{\mathrm{L}}}{\partial \mathrm{g}} = \frac{4 \, \dot{\mathrm{m}}_{\mathrm{L}}}{\pi \sqrt{\mathrm{g}} \, \mathrm{d}^{5} \, \rho_{\mathrm{L}} \left(\rho_{\mathrm{L}} - \rho_{\mathrm{G}} \right)} \left(\frac{-1}{2 \mathrm{g}^{3/2}} \right) \\ &\frac{\partial \mathrm{Fr}_{\mathrm{L}}}{\partial \mathrm{d}} = \frac{4 \, \dot{\mathrm{m}}_{\mathrm{L}}}{\pi \sqrt{\mathrm{g}} \, \rho_{\mathrm{L}} \left(\rho_{\mathrm{L}} - \rho_{\mathrm{G}} \right)} \left(\frac{-5}{2 \, \mathrm{d}^{7/2}} \right) \\ &\frac{\partial \mathrm{Fr}_{\mathrm{L}}}{\partial \rho_{\mathrm{L}}} = \frac{4 \, \dot{\mathrm{m}}_{\mathrm{L}}}{\pi \sqrt{\mathrm{g}} \, \mathrm{d}^{5}} \left(-\frac{2 \rho_{\mathrm{L}} - \rho_{\mathrm{G}}}{2 \left(\rho_{\mathrm{L}} \left(\rho_{\mathrm{L}} - \rho_{\mathrm{G}} \right) \right)^{3/2}} \right) \\ &\frac{\partial \mathrm{Fr}_{\mathrm{L}}}{\partial \rho_{\mathrm{G}}} = \frac{4 \, \dot{\mathrm{m}}_{\mathrm{L}}}{\pi \sqrt{\mathrm{g}} \, \mathrm{d}^{5}} \left(\frac{\rho_{\mathrm{L}}}{2 \left(\rho_{\mathrm{L}} \left(\rho_{\mathrm{L}} - \rho_{\mathrm{G}} \right) \right)^{3/2}} \right) \\ & \mathrm{w} \mathrm{Fr}_{\mathrm{L}} = \pm \left[\left(\frac{\partial \mathrm{Fr}_{\mathrm{L}}}{\partial \rho_{\mathrm{G}}} \, \mathrm{w}_{\mathrm{L}} \right)^{2} + \left(\frac{\partial \mathrm{Fr}_{\mathrm{L}}}{\partial \mathrm{g}} \, \mathrm{wg} \right)^{2} + \left(\frac{\partial \mathrm{Fr}_{\mathrm{L}}}{\partial \mathrm{d}} \, \mathrm{wd} \right)^{2} + \left(\frac{\partial \mathrm{Fr}_{\mathrm{L}}}{\partial \rho_{\mathrm{L}}} \, \mathrm{w\rho}_{\mathrm{L}} \right)^{2} \\ &+ \left(\frac{\partial \mathrm{Fr}_{\mathrm{L}}}{\partial \rho_{\mathrm{G}}} \, \mathrm{w\rho}_{\mathrm{G}} \right)^{2} \right]^{1/2} \end{aligned}$$

$$\frac{\mathrm{wFr}_{\mathrm{L}}}{\mathrm{Fr}_{\mathrm{L}}} = \pm \left[\left(\frac{\partial \mathrm{Fr}_{\mathrm{L}}}{\partial \dot{\mathrm{m}}_{\mathrm{L}}} \frac{\mathrm{w}\dot{\mathrm{m}}_{\mathrm{L}}}{\mathrm{Fr}_{\mathrm{L}}} \right)^{2} + \left(\frac{\partial \mathrm{Fr}_{\mathrm{L}}}{\partial g} \frac{\mathrm{w}g}{\mathrm{Fr}_{\mathrm{L}}} \right)^{2} + \left(\frac{\partial \mathrm{Fr}_{\mathrm{L}}}{\partial d} \frac{\mathrm{w}d}{\mathrm{Fr}_{\mathrm{L}}} \right)^{2} + \left(\frac{\partial \mathrm{Fr}_{\mathrm{L}}}{\partial \rho_{\mathrm{L}}} \frac{\mathrm{w}\rho_{\mathrm{L}}}{\mathrm{Fr}_{\mathrm{L}}} \right)^{2} + \left(\frac{\partial \mathrm{Fr}_{\mathrm{L}}}{\partial \rho_{\mathrm{G}}} \frac{\mathrm{w}\rho_{\mathrm{G}}}{\mathrm{Fr}_{\mathrm{L}}} \right)^{2}$$

$$\begin{split} \frac{wFr_L}{Fr_L} \\ &= \pm \left[\left(\frac{4}{\pi \sqrt{g \, d^5 \, \rho_L \, (\rho_L - \rho_G)}} \frac{\pi \sqrt{g \, d^5 \, \rho_L \, (\rho_L - \rho_G)}}{4 \, \dot{m}_L} w \dot{m}_L \right)^2 \\ &+ \left(\frac{4 \, \dot{m}_L}{\pi \sqrt{g \, \delta^5 \, \rho_L \, (\rho_L - \rho_G)}} \left(\frac{-1}{2g^{3/2}} \right) \frac{\pi \sqrt{g \, d^5 \, \rho_L \, (\rho_L - \rho_G)}}{4 \, \dot{m}_L} w g \right)^2 \\ &+ \left(\frac{4 \, \dot{m}_L}{\pi \sqrt{g \, \rho_L \, (\rho_L - \rho_G)}} \left(\frac{-5}{2 \, d^{7/2}} \right) \frac{\pi \sqrt{g \, d^5 \, \rho_L \, (\rho_L - \rho_G)}}{4 \, \dot{m}_L} w d \right)^2 \\ &+ \left(\frac{4 \, \dot{m}_L}{\pi \sqrt{g \, d^5}} \left(- \frac{2\rho_L - \rho_G}{2 \, \left(\rho_L (\rho_L - \rho_G) \right)^{3/2}} \right) \frac{\pi \sqrt{g \, d^5 \, \rho_L \, (\rho_L - \rho_G)}}{4 \, \dot{m}_L} w \rho_L \right)^2 \\ &+ \left(\frac{4 \, \dot{m}_L}{\pi \sqrt{g \, d^5}} \left(\frac{\rho_L}{2 \, \left(\rho_L (\rho_L - \rho_G) \right)^{3/2}} \right) \frac{\pi \sqrt{g \, d^5 \, \rho_L \, (\rho_L - \rho_G)}}{4 \, \dot{m}_L} w \rho_G \right)^2 \right]^{1/2} \\ &\frac{wFr_L}{Fr_L} = \pm \left[\left(\frac{w \dot{m}_L}{\dot{m}_L} \right)^2 + \left(\frac{-1}{2} \, \frac{wg}{g} \right)^2 + \left(\frac{-5}{2} \, \frac{wd}{d} \right)^2 + \left(- \frac{(2\rho_L - \rho_G) \, w \rho_L}{2\rho_L (\rho_L - \rho_G)} \right)^2 \\ &+ \left(\frac{1}{2} \frac{w \rho_G}{(\rho_L - \rho_G)} \right)^2 \right]^{1/2} \end{split}$$

The error in the density of liquid and error in gravitational acceleration was assumed negligible, $w\rho_L\simeq 0$ and $wg\simeq 0$.

$$\frac{\mathrm{wFr}_{\mathrm{L}}}{\mathrm{Fr}_{\mathrm{L}}} = \pm \left[\left(\frac{\mathrm{w\dot{m}}_{\mathrm{L}}}{\mathrm{\dot{m}}_{\mathrm{L}}} \right)^2 + \left(\frac{-5}{2} \frac{\mathrm{wd}}{\mathrm{d}} \right)^2 + \left(\frac{1}{2} \frac{\mathrm{w\rho}_{\mathrm{G}}}{(\rho_{\mathrm{L}} - \rho_{\mathrm{G}})} \right)^2 \right]^{1/2}$$
(B.15)

Vernier caliper was used to measure diameter of the branches having uncertainty interval of ± 0.01 mm.

B.10 Sample Calculation for Estimation of Uncertainty in the Data

The sample calculation is shown for the set no. 1-1.1.

B.10.1 Uncertainty in P_{TC}

The atmospheric pressure was noted with the help of barometer as,

Barometer reading = 29.52 inches of mercury.

The atmospheric pressure in bar was calculated as,

1 bar = 29.9213 inches of mercury (Perry's Chemical Engineers' Handbook, 1999)

 $P_{atm} = Barometer Reading \times \frac{1.01325}{29.9213}$

$$= 29.52 \times \frac{1.01325}{29.9213}$$

 $= 999.660 \times 10^{-3}$ bar ≈ 1.00 bar

The uncertainty in P_{TC} measurement by pressure transmitter was, $wP_{TC,T}\!=\pm$ 0.015 bar.

 $\frac{wP_{TC,T}}{P_{TC}} = \pm \left(\frac{0.015}{5.005} \times 100\right)$

$$= \pm 299.700 \%$$

The uncertainty in P_{TC} measurement due to fluctuation in process was $wP_{TC,P}{=}\pm 0.06$ bar

$$\frac{wP_{TC,P}}{P_{TC}} = \pm \left(\frac{0.06}{5.005} \times 100\right)$$
$$= \pm 1.199\%$$

The uncertainty in P_{TC} measurement due to uncertainty in pressure transmitter and fluctuation in process was calculated using equation (B.3):

$$\frac{wP_{TC}}{P_{TC}} = \pm \left(\left(\frac{wP_{TC,T}}{P_{TC}} \right)^2 + \left(\frac{wP_{TC,P}}{P_{TC}} \right)^2 \right)^{1/2} \times 100$$
$$= \pm \left(\left(\frac{0.015}{5.005} \right)^2 + \left(\frac{0.06}{5.005} \right)^2 \right)^{1/2} \times 100$$
$$= \pm 1.236 \%$$

$$wP_{TC} = \pm \left(\frac{1.236}{100} \times 5.005\right)$$

$$= \pm 61.862 \times 10^{-3}$$
 bar

B.10.2 Uncertainty in P_{TC,abs}

Absolute gas pressure in test chamber was calculated as follows,

The measured test chamber was $P_{TC} = 5.005$ bar.

 $P_{Tc,abs} = P_{TC} + P_{atm}$

$$= 5.005 + 1.00 = 6.005$$
 bar

 $wP_{atm} = 0$ (negligible)

: The uncertainty in $P_{TC,abs}$ measurement was, $wP_{TC,abs,T} = wP_{TC,T} = \pm 0.015$ bar.

$$\frac{wP_{TC,abs,T}}{P_{TC,abs}} = \pm \left(\frac{0.015}{6.005} \times 100\right)$$
$$= \pm 249.792 \times 10^{-3} \%$$

The uncertainty in $P_{TC,abs}$ measurement due to fluctuation in process was

 $wP_{TC,abs,P} = wP_{TC,P} = \pm 0.06 \text{ bar}$

$$\frac{\mathrm{wP}_{\mathrm{TC,abs,P}}}{\mathrm{P}_{\mathrm{TC,abs}}} = \pm \left(\frac{0.06}{6.005} \times 100\right)$$

$$= \pm 999.167 \times 10^{-3} \%$$

The uncertainty in P_{TC,abs} measurement due to uncertainty in pressure transmitter and fluctuation in process was calculated as follows:

$$\frac{wP_{TC,abs}}{P_{TC,abs}} = \pm \left(\left(\frac{wP_{TC,abs,T}}{P_{TC,abs}} \right)^2 + \left(\frac{wP_{TC,abs,P}}{P_{TC,abs}} \right)^2 \right)^{1/2} \times 100$$
$$= \pm \left(\left(\frac{0.015}{6.005} \right)^2 + \left(\frac{0.06}{6.005} \right)^2 \right)^{1/2} \times 100$$
$$= \pm 1.023 \%$$

 $wP_{TC,abs} = \pm \left(\frac{1.023}{100} \times 6.005\right)$

$$= \pm 61.431 \times 10^{-3}$$
 bar

B.10.3 Uncertainty in P_{PH}

Absolute gas pressure in phase separator was calculated using equation (B.4),

The measured phase separator pressure was $P_{PH} = 4.75$ bar.

 $P_{PH,abs} = P_{TC,T} + P_{atm}$

$$= 4.75 + 1.00$$

= 5.75 bar

The uncertainty in P_{PH} measurement by pressure transmitter was $wP_{PH,T}{=}\pm0.019$ bar

$$\frac{wP_{PH,T}}{P_{PH}} = \pm \left(\frac{0.019}{4.75} \times 100\right)$$
$$= \pm 0.400 \ \%$$

The uncertainty in P_{PH} due to fluctuation in the process was $wP_{PH,T} = \pm 0.02$ bar.

$$\frac{wP_{PH,P}}{P_{PH}} = \pm \left(\frac{0.02}{4.75} \times 100\right)$$
$$= \pm 0.421 \%$$

The uncertainty in P_{PH} due to pressure transmitter and fluctuation in the process was calculated as follows:

$$\frac{wP_{PH}}{P_{PH}} = \pm \left(\left(\frac{wP_{PH,T}}{P_{PH}} \right)^2 + \left(\frac{wP_{PH,P}}{P_{PH}} \right)^2 \right)^{1/2} \times 100$$
$$= \pm \left(\left(\frac{0.019}{4.75} \right)^2 + \left(\frac{0.02}{4.75} \right)^2 \right)^{1/2} \times 100$$
$$= \pm 0.581 \%$$
$$wP_{PH} = \pm \left(\frac{0.581}{100} \times 4.75 \right)$$

$$= \pm 27.598 \times 10^{-3}$$
 bar

B.10.4 Uncertainty in ΔP

The pressure difference between across the branch was calculated using equation (B.6).

$$\Delta P = P_{TC} - P_{PH}$$
$$= 5.005 - 4.75$$

= 0.255 bar

$$\frac{w\Delta P}{\Delta P} = \pm \left[\left(\frac{wP_{TC}}{(P_{TC} - P_{PH})} \right)^2 + \left(-\frac{wP_{PH}}{(P_{TC} - P_{PH})} \right)^2 \right]^{1/2} \times 100$$
$$= \pm \left[\left(\frac{61.862 \times 10^{-3}}{0.255} \right)^2 + \left(-\frac{27.598 \times 10^{-3}}{0.255} \right)^2 \right]^{1/2} X 100$$
$$= \pm 26.653 \%$$

 $w\Delta P = \pm \left(\frac{26.653}{100} \times \Delta P\right)$

$$= \pm \left(\frac{26.653}{100} \times 0.255\right)$$
$$= \pm 67.965 \times 10^{-3} \text{ bar}$$

B.10.5 Uncertainty in T_G

The gas temperature was noted down in the test section as,

$$T_{G} = 28.0 \ ^{0}C$$

= 28.0 + 273.15
= 301.15 K

The uncertainty of the thermometer was given as 1% of the Full Scale Deflection (FSD), and FSD was 50 0 C, therefore uncertainty in gas temperature measurement was calculated as follows,

$$wT_{G} = \pm 1\% \text{ of FSD}$$

$$= \pm \left(\frac{1}{100} (50 + 273.15)\right)$$

$$= \pm 3.232 \text{ K}$$

$$\frac{wT_{G}}{T_{G}} = \pm \left(\frac{3.232}{301.15} \times 100\right)$$

$$= \pm 10.73 \times 10^{-3} \%$$

B.10.6 Uncertainty in ρ_G

The gas constant was obtained from Perry's Chemical Engineers' Handbook (1999) as,

 $R_G = 287.15 \text{ kJ/kg. K}$

The density of gas obtained by treating the gas as ideal gas,

$$\rho_{\rm G} = \left(\frac{P_{\rm Tc,abs}}{R_{\rm G} T_{\rm G}}\right)$$
$$= \left(\frac{6.005 \times 10^5}{287.15 \times 301.15}\right)$$
$$= 6.944 \text{ kg/m}^3$$

The uncertainty in the density of gas was obtained using equation (B.8) as,

$$\begin{split} \frac{w\rho_G}{\rho_G} &= \pm \left[\left(\frac{wP_{TC,abs}}{P_{TC,abs}} \right)^2 + \left(-\frac{wT_G}{T_G} \right)^2 \right]^{1/2} \times 100 \\ &= \pm \left[\left(\frac{61.431 \times 10^{-3}}{6.005} \right)^2 + \left(-\frac{3.23}{301.15} \right)^2 \right]^{1/2} \times 100 \\ &= \pm 1.482 \times 10^{-3} \% \\ w\rho_G &= \pm \left(\frac{1.482 \times 10^{-3}}{100} \times \rho_G \right) \\ &= \pm \left(\frac{1.482 \times 10^{-3}}{100} \times 6.944 \right) \\ &= \pm 102.910 \times 10^{-3} \text{ kg/m}^3 \end{split}$$

B.10.7 Uncertainty in $\Delta \rho$

The density of liquid (at $T_G = 28.0$ ⁰C) was obtained from Perry's Chemical Engineers' Handbook (1999) as,

$$\rho_{\rm L} = 996.233 \text{ kg/m}^3$$

The difference in density of liquid and gas was calculated as,

$$\Delta \rho = \rho_{\rm L} - \rho_{\rm G}$$

= 996.233 - 6.944
= 989.289 kg/ m³

The uncertainty in the $\Delta \rho$ was calculated using equation (B.10),

$$\frac{w\Delta\rho}{\Delta\rho} = \pm \left[\left(-\frac{w\rho_G}{\Delta\rho} \right)^2 \right]^{1/2} \times 100$$
$$= \pm \left[\left(-\frac{102.910 \times 10^{-3}}{989.289} \right)^2 \right]^{1/2} \times 100$$
$$= \pm 10.199 \times 10^{-3} \%$$
$$w\Delta\rho = \pm \left(\frac{\Delta\rho \times 10.199 \times 10^{-3}}{100} \right)$$
$$= \pm \left(\frac{989.289 \times 10.199 \times 10^{-3}}{100} \right)$$
$$= \pm 100.898 \times 10^{-3} \text{ kg/m}^3$$

B.10.8 Uncertainty in m_L

The mass flow rate of liquid was measured by the flow meter as,

 $\dot{m}_{L,T} = 7.42 \text{ kg/min}$

The uncertainty in mass flow measurement due to flow transmitter in percentage was calculated using equation (B.12) as,

$$\frac{\mathrm{w}\dot{\mathrm{m}}_{\mathrm{L,T}}}{\dot{\mathrm{m}}_{\mathrm{L}}} = \pm \left(0.05 + \left(\frac{12 - \dot{\mathrm{m}}_{\mathrm{L}}}{30}\right) + \left(\frac{9}{1000 \times \dot{\mathrm{m}}_{\mathrm{L}}}\right)\right)$$

$$= \pm \left(0.05 + \left(\frac{12 - 7.42}{30} \right) + \left(\frac{9}{1000 \times 7.42} \right) \right)$$
$$= \pm 203.880 \times 10^{-3} \%$$
$$\therefore \text{ wm}_{\text{L,T}} = \pm \left(\frac{203.880 \times 10^{-3}}{100} \times 7.42 \right)$$
$$= \pm 15.128 \times 10^{-3} \text{ kg/min}$$

The mass flow rate was measured with the fluctuation of ± 0.1 kg/min in process,

 $\therefore w\dot{m}_{L,P} = \pm 0.1 \text{ kg/min}$

The uncertainty due to the fluctuation in process was calculated as,

$$\frac{\dot{\text{wm}}_{\text{L,P}}}{\dot{\text{m}}_{\text{L}}} = \pm \left(\frac{0.1}{7.42} \times 100\right)$$
$$= \pm 1.348 \ \%$$

The uncertainty in mass flow rate including the uncertainty of flow transmitter and uncertainty due to the fluctuation in process was calculated as follows,

$$\frac{w\dot{m}_{L}}{\dot{m}_{L}} = \pm \left(\sqrt{\left(\frac{w\dot{m}_{L,T}}{\dot{m}_{L}}\right)^{2} + \left(\frac{w\dot{m}_{L,P}}{\dot{m}_{L}}\right)^{2}} \right) \times 100$$

$$\frac{w\dot{m}_{L}}{\dot{m}_{L}} = \pm \left(\sqrt{\left(\frac{203.880 \times 10^{-3}}{100}\right)^{2} + \left(\frac{1.348}{100}\right)^{2}} \right) \times 100$$

$$= \pm 1.36 \%$$

$$w\dot{m}_{L} = \pm \left(\frac{1.36}{100} \times \dot{m}_{L}\right)$$

$$= \pm \left(\frac{1.36}{100} \times 7.42\right)$$
$$= \pm 100.912 \times 10^{-3} \text{ kg/min}$$

B.10.9 Uncertainty in d

The uncertainty in the branch diameter of 9.0 mm was calculated as,

$$\frac{\mathrm{wd}}{\mathrm{d}} = \pm \left(\frac{0.01}{9.0} \times 100\right)$$
$$= \pm 0.111\%$$

B.10.10 Uncertainty in Fr_L

The uncertainty in the Froude number was calculated by using equation (B.15) for the calculated $Fr_L = 6.58$,

$$\begin{split} \frac{\text{wFr}_{\text{L}}}{\text{Fr}_{\text{L}}} &= \pm \left[\left(\frac{\text{wm}_{\text{L}}}{\text{m}_{\text{L}}} \right)^2 + \left(\frac{-5}{2} \frac{\text{wd}}{\text{d}} \right)^2 + \left(\frac{1}{2} \frac{\text{w}\rho_{\text{G}}}{(\rho_{\text{L}} - \rho_{\text{G}})} \right)^2 \right]^{1/2} \times 100 \\ &= \pm \left[(1.36)^2 + \left(\frac{-5}{2} \times 0.111 \right)^2 + \left(\frac{1}{2} \times 102.910 \times 10^{-3} \right)^2 \right]^{\frac{1}{2}} \\ &= \pm 1.389 \% \\ \text{wFr}_{\text{L}} &= \pm \left(\frac{1.389}{100} \times 6.58 \right) \\ &= \pm 91.396 \times 10^{-3} \end{split}$$

Appendix C

Experimental Data

Series no. 1-1 P _{atm} = 1.00 bar						
Set	TG		Activa	ated line	e	
no.	(°C)	B1				
		Fr _{L,B1}	P _{TC} (bar)	ΔP (bar)	h _{OGE,B1} d	
1-1.1 1-1.2 1-1.3 1-1.4 1-1.5 1-1.6 1-1.7 1-1.8	28.0 36.0 25.3 32.5 28.0 31.0 27.5 22.5	6.58 9.31 11.22 12.93 18.54 22.62 25.88 27.29	5.005 5.021 4.998 5.009 5.017 5.005 6.004 6.002	0.255 0.531 0.748 1.009 2.027 3.005 3.994 4.492	1.19 1.44 1.50 1.61 1.81 1.99 2.07 2.10	

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	Series no. 1-3 P _{atm} = 1.00 bar						
Set T _c Activated line					e		
no.	(°C)		B3				
		Fr _{L,B3}	P _{TC} (bar)	ΔP (bar)	h _{OGE,B3} d		
1-2.1 1-2.2 1-2.3 1-2.4 1-2.5 1-2.6 1-2.7 1-2.8	28.5 36.0 25.5 32.5 28.5 31.0 28.0 24.5	6.52 9.08 11.23 12.96 18.53 22.57 25.89 27.30	4.999 5.000 5.014 5.016 5.004 5.996 6.002	0.249 0.500 0.750 1.014 2.026 2.994 3.996 4.492	1.03 1.23 1.37 1.56 1.90 2.04 2.18 2.26		

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Series no. 1-2 P _{atm} = 1.00 bar						
Set	T _G		Activated line			
no.	(⁰C)		B2			
		Fr _{L,B2}	P _{TC} (bar)	ΔP (bar)	$\frac{h_{OGE,B2}}{d}$	
1-3.1	28.0	6.53	5.000	0.250	1.27	
1-3.2	36.0	9.14	5.009	0.509	1.52	
1-3.3	25.5	11.23	5.000	0.750	1.61	
1-3.4	32.5	12.88	4.992	1.002	1.69	
1-3.5	28.0	18.44	5.014	2.004	1.97	
1-3.6	31.0	22.69	5.028	3.018	2.25	
1-3.7	27.5	25.90	5.999	3.999	2.37	
1-3.8	22.5	27.35	6.013	4.513	2.48	

	Series no. 1-4
	$P_{atm} = 1.00 \text{ bar}$
Tc	Activated line

Set	T _G	Tetrvated line			
no.	(°C)	B4			
		Fr _{L,B4}	P _{TC} (bar)	ΔP (bar)	h _{OGE,B4} d
$1-4.1 \\ 1-4.2 \\ 1-4.3 \\ 1-4.4 \\ 1-4.5 \\ 1-4.6 \\ 1-4.7 \\ 1-4.8 $	28.5 36.0 25.8 32.5 29.0 31.0 27.5 23.5	6.37 9.16 11.25 12.95 18.44 22.65 25.88 27.32	4.996 5.001 5.002 5.012 5.003 5.000 5.992 6.001	0.236 0.511 0.752 1.012 2.003 3.010 3.992 4.501	1.42 1.53 1.67 1.76 2.07 2.26 2.35 2.49

Т	able C.1	: Experimental	data for	single	discharge	(cont.)

	Series no. 1-5 P _{atm} = 1.00 bar						
Set	TG		Activa	ated line	e		
no.	(°C)		B5				
		Fr _{L,B5}	P _{TC} (bar)	ΔP (bar)	h _{OGE,B5} d		
$ \begin{array}{c} 1-5.1 \\ 1-5.2 \\ 1-5.3 \\ 1-5.4 \\ 1-5.5 \\ 1-5.6 \\ 1-5.7 \\ 1-5.8 \\ \end{array} $	28.5 36.0 25.5 32.5 29.0 31.0 27.5 23.5	6.57 9.08 11.27 12.92 18.54 22.60 25.88 27.31	5.004 5.001 5.005 5.007 5.016 4.999 6.002 5.997	0.254 0.501 0.755 1.007 2.026 2.999 3.992 4.497	1.21 1.29 1.44 1.46 1.78 1.92 2.04 2.07		

	Series no. 2-1												
	$P_{atm} = 1.00 \text{ bar}$												
Set	T _G				Activat	ed lines							
no.	(°Č)]	B1]	B2					
		Fr _{L,B1}	P _{TC1} (bar)	ΔP (bar)	$\frac{h_{OGE,B1}}{d}$	Fr _{L,B2}	P _{TC2} (bar)	ΔP (bar)	$\frac{h_{OGE,B2}}{d}$				
2-1.1 2-1.2 2-1.3 2-1.4 2-1.5 2-1.6 2-1.7 2-1.8	27.5 32.0 25.0 31.5 31.0 30.5 28.5 25.0	6.57 9.15 11.24 12.84 18.43 22.57 25.92 27.40	5.004 5.012 5.001 4.996 5.018 4.995 6.002 6.023	0.254 0.512 0.751 0.996 1.998 2.995 4.002 4.523	1.24 1.44 1.61 1.70 2.02 2.25 2.33 2.36	6.53 9.01 11.30 12.97 18.42 22.57 25.85 27.37	4.990 5.003 5.000 4.996 4.995 5.005 5.993 6.005	0.250 0.493 0.760 1.016 1.995 2.995 3.983 4.515	$ \begin{array}{c} 1.16\\ 1.24\\ 1.32\\ 1.41\\ 1.63\\ 1.80\\ 1.92\\ 2.03 \end{array} $				

Table C.2 : Experimental	data for	dual	discharge
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					<i>Series no</i> . P _{atm} = 1.00	2-2) bar			
Set	T _G				Activat	ed lines			
no.	(°Č)]	B1]	B3	
		Fr _{L,B1}	P _{TC1} (bar)	ΔP (bar)	$\frac{h_{OGE,B1}}{d}$	Fr _{L,B3}	P _{TC3} (bar)	ΔP (bar)	$\frac{h_{OGE,B3}}{d}$
2-2.1 2-2.2 2-2.3 2-2.4 2-2.5 2-2.6 2-2.7 2-2.8	24.0 34.0 24.0 31.8 32.0 31.3 29.0 25.5	6.60 9.03 11.36 13.30 18.42 22.60 25.99 27.31	5.007 4.995 5.020 5.050 4.994 5.020 6.010 5.995	$\begin{array}{c} 0.257\\ 0.495\\ 0.770\\ 1.070\\ 1.994\\ 3.000\\ 4.020\\ 4.495 \end{array}$	1.13 1.41 1.53 1.67 1.90 2.10 2.27 2.33	6.52 9.00 11.28 12.85 18.43 22.50 26.06 27.28	5.000 4.981 5.008 4.997 4.997 4.987 6.031 5.985	0.250 0.491 0.758 0.997 1.997 2.977 4.041 4.485	1.00 1.23 1.34 1.50 1.78 2.07 2.15 2.26

	Series no. 2-3												
	$P_{atm} = 1.00 \text{ bar}$												
Set	T _G		Activated lines										
no.	(°Č)]	B1]	B4					
		Fr _{L,B1}	P _{TC} (bar)	ΔP (bar)	$\frac{h_{OGE,B1}}{d}$	Fr _{L,B4}	P _{TC} (bar)	ΔP (bar)	$\frac{h_{OGE,B4}}{d}$				
2-3.1 2-3.2 2-3.3 2-3.4 2-3.5 2-3.6 2-3.7 2-3.8	25.0 33.0 24.5 31.5 32.0 31.0 28.5 25.5	6.46 9.20 11.27 13.19 18.37 22.67 25.93 27.32	4.995 5.018 5.006 5.011 5.003 5.035 6.006 5.997	0.245 0.518 0.756 1.051 1.983 3.015 4.006 4.497	1.19 1.41 1.53 1.70 1.99 2.22 2.33 2.36	6.51 9.02 11.29 12.32 18.43 22.72 25.96 27.32	4.999 5.003 5.009 5.002 5.006 5.015 6.003 5.996	0.249 0.493 0.759 0.912 1.996 3.025 4.013 4.496	1.31 1.62 1.67 1.81 2.04 2.26 2.38 2.43				

Table C.2 : Ex	perimental	data for	dual	discharge	(cont.))
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					Series no. $P_{atm} = 1.00$	2-4 0 bar					
Set	TG		Activated lines								
no.	(°C)]	B1]	B5			
		Fr _{L,B1}	P _{TC} (bar)	ΔP (bar)	$\frac{h_{OGE,B1}}{d}$	Fr _{L,B5}	P _{TC} (bar)	ΔP (bar)	$\frac{h_{OGE,B5}}{d}$		
2-4.1 2-4.2 2-4.3 2-4.4 2-4.5 2-4.6 2-4.7 2-4.8	27.5 32.0 25.0 31.5 29.5 30.0 28.1 24.5	6.51 9.11 11.23 12.88 18.37 22.63 25.95 27.33	4.999 5.006 5.000 5.002 4.995 5.007 6.003 6.011	0.249 0.506 0.750 1.002 1.985 3.007 4.013 4.501	1.10 1.33 1.44 1.64 1.87 2.02 2.16 2.22	6.58 9.12 11.23 12.91 18.44 22.60 25.96 27.36	5.005 5.007 5.000 5.007 5.003 5.001 6.004 6.012	0.255 0.507 0.750 1.007 2.003 3.001 4.014 4.512	$ \begin{array}{r} 1.18\\ 1.35\\ 1.46\\ 1.61\\ 1.89\\ 2.04\\ 2.15\\ 2.18\\ \end{array} $		

	Series no. 2-5 $P_{stm} = 1.00 \text{ bar}$												
	$P_{atm} = 1.00 \text{ bar}$												
Set	T _G		Activated lines										
no.	(°Č)]	B2]	B3					
		Fr _{L,B2}	P _{TC} (bar)	ΔP (bar)	$\frac{h_{OGE,B2}}{d}$	Fr _{L,B3}	P _{TC} (bar)	ΔP (bar)	h _{OGE,B3} d				
2-5.1 2-5.2 2-5.3 2-5.4 2-5.5 2-5.6 2-5.7 2-5.8	25.5 36.0 23.5 31.5 33.0 31.5 29.0 27.0	6.50 9.11 11.28 13.07 18.60 22.72 25.96 27.33	4.998 5.014 5.008 5.023 5.007 5.034 6.014 5.997	0.248 0.504 0.758 1.033 2.037 3.024 4.014 4.497	1.38 1.61 1.77 1.97 2.48 2.71 2.85 2.99	6.61 9.15 11.23 12.79 18.49 22.72 25.93 27.34	4.998 5.010 5.000 5.007 5.020 5.014 6.023 5.990	0.258 0.510 0.750 0.987 2.010 3.024 4.003 4.500	1.11 1.39 1.53 1.76 2.01 2.35 2.46 2.63				

Table C.2 : Ex	perimental	data for	dual	discharge	(cont.))
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	Series no. 2-6												
	$P_{atm} = 1.00 \text{ bar}$												
Set	T _G		Activated lines										
no.	(°C)]	B2]	B4					
		Fr _{L,B2}	P _{TC} (bar)	ΔP (bar)	$\frac{h_{OGE,B2}}{d}$	Fr _{L,B4}	P _{TC} (bar)	ΔP (bar)	$\frac{h_{OGE,B4}}{d}$				
2-6.1 2-6.2 2-6.3 2-6.4 2-6.5 2-6.6 2-6.7 2-6.8	26.5 36.0 25.0 31.5 31.0 30.0 28.1 24.5	6.54 9.19 11.22 12.81 18.37 22.58 25.90 27.40	5.001 5.015 4.998 4.991 4.985 5.007 5.998 6.016	0.251 0.515 0.748 0.991 1.985 2.997 3.998 4.526	1.46 1.58 1.80 1.83 2.20 2.48 2.60 2.71	6.54 9.28 11.22 12.81 18.53 22.47 25.96 27.35	5.001 5.017 4.999 4.991 5.013 4.974 6.014 6.008	0.251 0.527 0.749 0.991 2.023 2.974 4.014 4.508	1.64 1.73 1.90 1.95 2.15 2.32 2.43 2.52				

	Series no. 2-7 $P_{-} = 1.00 \text{ bar}$												
	$P_{\rm atm} = 1.00 \text{bar}$												
Set	TG		Activated lines										
no.	(°Č)]	B2]	B5					
		Fr _{L,B2}	P _{TC} (bar)	ΔP (bar)	$\frac{h_{OGE,B2}}{d}$	Fr _{L,B5}	P _{TC} (bar)	ΔP (bar)	h _{OGE,B5} d				
2-7.1 2-7.2 2-7.3 2-7.4 2-7.5 2-7.6 2-7.7 2-7.8	24.5 35.0 24.0 31.5 32.0 31.0 29.5 26.5	6.41 9.13 11.21 12.41 18.39 22.75 25.99 27.33	5.000 5.007 4.997 4.997 4.998 5.031 6.011 5.988	0.240 0.507 0.747 0.927 1.988 3.031 4.021 4.498	1.38 1.52 1.63 1.80 2.14 2.37 2.54 2.57	6.58 8.94 11.17 12.81 18.40 22.69 25.87 27.29	5.005 4.992 5.002 5.001 4.990 5.019 5.997 5.985	0.255 0.482 0.742 0.991 1.990 3.019 3.987 4.485	1.23 1.46 1.58 1.69 1.95 2.18 2.30 2.47				

Table C.2 : Ex	perimental	data for	dual	discharge	(cont.)	
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	Series no. 2-8 $P_{atm} = 1.00 \text{ bar}$												
Set	TG		Activated lines										
no.	(°C)]	B3]	B4					
		Fr _{L,B3}	P _{TC} (bar)	ΔP (bar)	h _{OGE,B3} d	Fr _{L,B4}	P _{TC} (bar)	ΔP (bar)	$\frac{h_{OGE,B4}}{d}$				
2-8.1 2-8.2 2-8.3 2-8.4 2-8.5 2-8.6 2-8.7 2-8.8	25.0 36.0 23.5 31.5 34.0 31.5 29.0 27.0	6.52 8.96 11.25 12.79 18.43 22.59 25.90 27.35	5.010 4.984 5.003 4.998 5.004 4.996 5.995 5.993	0.250 0.484 0.753 0.988 1.994 2.996 3.995 4.503	1.11 1.42 1.56 1.78 2.12 2.35 2.43 2.57	6.51 9.07 11.23 12.67 18.38 22.52 25.94 27.32	4.999 4.999 5.001 4.978 4.993 5.011 5.998 6.005	0.249 0.499 0.751 0.968 1.983 2.981 4.008 4.495	1.50 1.62 1.81 1.95 2.32 2.63 2.69 2.95				

	Series no. 2-9												
	$P_{atm} = 1.00 \text{ bar}$												
Set T _G Activated lines													
no.	(°Č)]	B3]	B5					
		Fr _{L,B3}	P _{TC} (bar)	ΔP (bar)	h _{OGE,B3} d	Fr _{L,B5}	P _{TC} (bar)	ΔP (bar)	h _{OGE,B5} d				
2-9.1 2-9.2 2-9.3 2-9.4 2-9.5 2-9.6 2-9.7 2-9.8	23.5 35.5 23.5 31.8 32.5 31.5 29.0 26.5	6.60 9.17 11.20 12.86 18.46 22.70 25.67 27.37	4.997 5.012 4.996 4.999 4.994 5.020 5.980 6.010	0.257 0.512 0.746 0.999 2.004 3.020 3.930 4.510	$ \begin{array}{r} 1.00\\ 1.25\\ 1.34\\ 1.53\\ 1.78\\ 2.04\\ 2.15\\ 2.26\\ \end{array} $	6.53 9.20 11.20 12.96 18.41 22.45 25.90 27.38	5.001 5.007 4.996 4.995 4.992 4.977 5.996 6.014	0.251 0.517 0.746 1.015 1.992 2.967 3.996 4.514	1.12 1.38 1.46 1.66 1.92 2.10 2.18 2.27				

Table C.2 : Ex	perimental	data for	dual	discharge	(cont.)	
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	Series no. 2-10 P _{atm} = 1.00 bar													
Set	T _G		Activated lines											
no.	(°Č)]	B4]	B5						
		Fr _{L,B4}	P _{TC} (bar)	ΔP (bar)	$\frac{h_{OGE,B4}}{d}$	Fr _{L,B5}	P _{TC} (bar)	ΔP (bar)	h _{OGE,B5} d					
2-10.1 2-10.2 2-10.3 2-10.4 2-10.5 2-10.6 2-10.7 2-10.8	26.5 35.0 25.0 31.5 31.0 30.5 29.0 25.5	6.51 9.16 11.36 12.82 18.51 22.60 25.88 27.25	4.999 5.001 5.009 4.993 5.007 5.010 5.991 5.985	0.249 0.511 0.769 0.993 2.017 3.000 3.991 4.475	$ \begin{array}{r} 1.25 \\ 1.31 \\ 1.45 \\ 1.50 \\ 1.70 \\ 1.84 \\ 1.98 \\ 2.01 \\ \end{array} $	6.55 9.16 11.34 12.50 18.28 22.57 25.88 27.35	5.002 5.011 5.006 4.991 4.992 5.003 5.990 6.016	0.252 0.511 0.766 0.941 1.962 2.993 3.990 4.506	1.15 1.35 1.52 1.64 1.89 2.04 2.30 2.33					

	Series no. 3-1												
	$P_{atm} = 1.00 \text{ bar}$												
Set	T _G	Activated lines											
no.	(°C)	B1]	32]	B3	
		Fr _{L,B1}	P _{TC} (bar)	ΔP (bar)	$\frac{h_{OGE,B1}}{d}$	Fr _{L,B2}	P _{TC} (bar)	ΔP (bar)	$\frac{h_{OGE,B2}}{d}$	Fr _{L,B3}	P _{TC} (bar)	ΔP (bar)	$\frac{h_{OGE,B3}}{d}$
3-1.1 3-1.2 3-1.3 3-1.4 3-1.5 3-1.6 3-1.7 3-1.8	20.5 28.5 23.0 31.0 30.5 31.5 29.0 27.5	6.48 8.92 11.11 12.74 18.39 22.47 25.82 27.37	4.997 4.992 4.993 5.030 4.989 4.992 5.992 6.008	0.247 0.482 0.733 0.980 1.989 2.972 3.972 4.508	1.21 1.53 1.67 1.81 2.19 2.36 2.59 2.68	6.49 9.15 11.25 12.66 18.49 22.65 25.88 27.31	4.998 5.022 4.994 4.997 5.004 5.010 5.989 5.999	0.248 0.512 0.754 0.967 2.014 3.010 3.989 4.489	1.24 1.38 1.52 1.69 2.03 2.28 2.45 2.54	6.54 9.52 11.36 13.07 18.46 22.63 26.04 27.37	5.002 5.022 5.010 5.042 5.007 5.005 6.014 6.009	$\begin{array}{c} 0.252\\ 0.562\\ 0.770\\ 1.032\\ 2.007\\ 3.005\\ 4.034\\ 4.509 \end{array}$	1.03 1.34 1.53 1.73 2.04 2.32 2.40 2.54

	Series no. 3-2												
	P _{atm} = 1.00 bar												
Set	TG		Activated lines										
no.	(°Č)]	B1]	B2]	B4	
		Fr _{L,B1}	P _{TC} (bar)	ΔP (bar)	$\frac{h_{OGE,B1}}{d}$	Fr _{L,B2}	P _{TC} (bar)	ΔP (bar)	$\frac{h_{OGE,B2}}{d}$	Fr _{L,B4}	P _{TC} (bar)	ΔP (bar)	h _{OGE,B4} d
3-2.1 3-2.2 3-2.3 3-2.4 3-2.5 3-2.6 3-2.7 3-2.8	20.0 29.5 21.0 30.3 29.5 31.0 27.5 27.5	6.54 9.02 11.23 12.86 18.60 22.72 25.90 27.40	5.002 5.005 5.002 5.009 5.020 5.026 5.998 6.018	0.252 0.495 0.752 0.999 2.040 3.026 3.998 4.518	1.21 1.47 1.64 1.79 2.04 2.25 2.36 2.51	6.62 8.98 11.28 12.92 18.39 22.83 25.83 27.33	5.009 4.990 5.009 5.019 4.991 5.009 5.990 6.007	0.259 0.490 0.759 1.009 1.991 3.049 3.980 4.497	1.13 1.24 1.38 1.55 1.77 1.92 2.11 2.34	6.63 9.11 11.20 12.84 18.42 22.60 25.87 27.36	5.000 5.007 4.997 4.997 4.997 4.990 5.999 5.994	0.260 0.507 0.747 0.997 1.997 3.000 3.989 4.504	$ \begin{array}{r} 1.50\\ 1.76\\ 1.90\\ 1.90\\ 2.15\\ 2.32\\ 2.52\\ 2.60\\ \end{array} $

	Series no. 3-3												
	$P_{atm} = 1.00 \text{ bar}$												
Set	T _G		Activated lines										
no.	(°C)	B1]	32			B5		
		Fr _{L,B1}	P _{TC} (bar)	ΔP (bar)	$\frac{h_{OGE,B1}}{d}$	Fr _{L,B2}	P _{TC} (bar)	ΔP (bar)	$\frac{h_{OGE,B2}}{d}$	Fr _{L,B5}	P _{TC} (bar)	ΔP (bar)	h _{OGE,B5} d
3-3.1 3-3.2 3-3.3 3-3.4 3-3.5 3-3.6 3-3.7 3-3.8	19.5 31.0 21.5 31.5 28.0 31.5 26.5 27.5	6.54 9.11 11.22 12.93 18.37 22.28 25.91 27.32	5.002 5.006 5.000 5.010 4.997 5.000 6.004 6.001	0.252 0.506 0.750 1.010 1.987 2.930 4.004 4.491	1.30 1.44 1.67 1.79 2.07 2.22 2.36 2.48	6.56 9.03 11.27 12.70 18.34 22.32 25.86 27.35	5.004 4.995 5.007 4.993 5.000 5.000 5.998 6.001	0.254 0.495 0.757 0.973 1.980 2.940 3.988 4.501	$ \begin{array}{r} 1.10\\ 1.18\\ 1.27\\ 1.38\\ 1.61\\ 1.80\\ 1.89\\ 2.00\\ \end{array} $	6.49 9.11 11.22 12.80 18.44 22.63 25.90 27.30	4.998 5.006 5.000 4.979 5.005 5.006 6.001 6.005	0.248 0.506 0.750 0.989 2.005 3.006 4.001 4.485	1.18 1.44 1.52 1.72 2.01 2.12 2.36 2.64

Table C.3 : Experimental data for triple discharge (cont.)

	Series no. 3-4													
						Pa	$_{tm} = 1.0$	00 bar						
Set	TG						Activa	ted line	es					
no.	(°Č)	B1]	33			B4			
		Fr _{L,B1}	P _{TC} (bar)	ΔP (bar)	h _{OGE,B1} d	Fr _{L,B3}	P _{TC} (bar)	ΔP (bar)	h _{OGE,B3} d	Fr _{L,B4}	P _{TC} (bar)	ΔP (bar)	h _{OGE,B4} d	
3-4.1 3-4.2 3-4.3 3-4.4 3-4.5 3-4.6 3-4.7 3-4.8	21.5 28.0 24.5 28.5 30.5 28.3 25.3 27.5	6.49 9.62 11.25 12.85 18.38 22.59 25.94 27.37	4.998 5.066 5.003 5.009 5.016 5.002 6.015 6.009	0.248 0.576 0.753 0.999 1.986 3.002 4.015 4.509	1.19 1.53 1.56 1.84 2.13 2.42 2.53 2.62	6.49 9.46 11.34 12.78 18.39 22.59 25.93 27.34	4.998 5.005 5.006 4.998 4.989 5.002 6.011 5.998	0.248 0.555 0.766 0.988 1.989 3.002 4.011 4.498	1.09 1.39 1.53 1.76 2.09 2.29 2.49 2.63	6.47 9.23 11.22 12.85 18.47 22.60 25.87 27.34	4.996 5.023 4.998 4.999 5.008 5.004 6.004 5.998	0.246 0.523 0.748 0.999 2.008 3.004 3.994 4.498	1.59 1.76 1.87 1.90 2.32 2.55 2.72 2.80	
	Series no. 3-5													
--	--	--	--	--	--	--	--	--	--	--	--	--	--	
	$P_{atm} = 1.00 \text{ bar}$													
Set	T _G						Activa	ted line	es					
no.	(°Č)	B1 B3 B5												
		Fr _{L,B1}	P _{TC} (bar)	ΔP (bar)	$\frac{h_{OGE,B1}}{d}$	Fr _{L,B3}	P _{TC} (bar)	ΔP (bar)	$\frac{h_{OGE,B3}}{d}$	Fr _{L,B5}	P _{TC} (bar)	ΔP (bar)	$\frac{h_{OGE,B5}}{d}$	
3-5.1 3-5.2 3-5.3 3-5.4 3-5.5 3-5.6 3-5.7 3-5.8	23.0 29.0 23.8 31.0 30.0 31.5 25.0 27.5	6.52 8.95 11.26 12.88 18.44 22.54 25.90 27.36	5.000 4.976 5.005 5.002 4.993 4.996 6.004 6.005	0.250 0.486 0.755 1.002 2.003 2.986 4.004 4.505	1.13 1.27 1.47 1.73 2.02 2.22 2.33 2.42	6.60 9.40 11.17 12.75 18.43 22.66 25.90 27.34	5.002 5.046 4.992 5.002 5.000 5.002 6.003 6.000	$\begin{array}{c} 0.257\\ 0.546\\ 0.742\\ 0.982\\ 2.000\\ 3.012\\ 4.003\\ 4.500 \end{array}$	0.98 1.20 1.34 1.42 1.70 2.01 2.09 2.23	6.50 8.83 11.22 12.94 18.42 22.59 25.92 27.26	4.998 4.989 4.999 5.002 4.997 5.006 6.010 5.993	0.248 0.469 0.749 1.012 1.997 2.996 4.010 4.473	1.18 1.32 1.55 1.66 2.07 2.36 2.27 2.64	

	Series no. 3-6												
	$P_{atm} = 1.00 \text{ bar}$												
Set	TG						Activa	ted line	es				
no.	(°C)]	B1]	34]	B5	
		Fr _{L,B1}	P _{TC} (bar)	ΔP (bar)	$\frac{h_{OGE,B1}}{d}$	Fr _{L,B4}	P _{TC} (bar)	ΔP (bar)	$\frac{h_{OGE,B4}}{d}$	Fr _{L,B5}	P _{TC} (bar)	ΔP (bar)	$\frac{h_{OGE,B5}}{d}$
3-6.1 3-6.2 3-6.3 3-6.4 3-6.5 3-6.6 3-6.7 3-6.8	19.5 30.0 24.5 28.5 29.0 28.3 26.0 27.5	6.49 9.03 11.26 13.04 18.60 22.47 25.90 27.35	4.998 5.006 5.005 5.020 5.011 4.995 6.011 6.002	0.248 0.496 0.755 1.030 2.041 2.975 4.001 4.502	$ \begin{array}{r} 1.16\\ 1.41\\ 1.50\\ 1.64\\ 2.10\\ 2.30\\ 2.33\\ 2.45 \end{array} $	6.66 9.18 11.17 12.84 18.47 22.57 25.98 27.33	5.013 5.016 4.992 4.998 5.000 4.998 6.013 5.995	0.263 0.516 0.742 0.998 2.010 2.998 4.023 4.495	1.25 1.34 1.39 1.45 1.64 1.79 1.87 1.90	6.54 9.03 11.22 12.83 18.50 22.47 25.91 27.34	5.002 5.006 4.999 4.996 5.008 4.995 6.013 6.000	0.252 0.496 0.749 0.996 2.018 2.975 4.003 4.500	1.21 1.35 1.55 1.72 2.15 2.30 2.33 2.47

	Series no. 3-7												
	$P_{atm} = 1.00 \text{ bar}$												
Set	T _G						Activa	ted line	es				
no.	(°Č)]	B2]	33]	B4	
		Fr _{L,B2}	P _{TC} (bar)	ΔP (bar)	$\frac{h_{OGE,B2}}{d}$	Fr _{L,B3}	P _{TC} (bar)	ΔP (bar)	h _{OGE,B3} d	Fr _{L,B4}	P _{TC} (bar)	ΔP (bar)	$\frac{h_{OGE,B4}}{d}$
3-7.1 3-7.2 3-7.3 3-7.4 3-7.5 3-7.6 3-7.7 3-7.8	24.5 28.0 24.8 28.0 30.5 28.5 25.0 27.5	6.67 8.95 11.30 12.81 18.29 22.62 25.85 27.35	5.003 4.976 5.011 4.993 5.005 5.018 5.998 6.003	0.263 0.486 0.761 0.993 1.965 3.008 3.988 4.503	1.63 1.72 1.92 2.08 2.51 2.82 3.05 3.16	6.60 8.86 11.36 13.05 18.46 22.63 26.03 27.43	4.997 5.024 5.009 5.011 5.006 5.000 6.009 5.999	$\begin{array}{c} 0.257\\ 0.474\\ 0.769\\ 1.031\\ 2.006\\ 3.010\\ 4.039\\ 4.529\end{array}$	$ \begin{array}{c} 1.20\\ 1.56\\ 1.70\\ 1.95\\ 2.46\\ 2.60\\ 2.80\\ 3.00\\ \end{array} $	6.68 8.86 11.31 12.94 18.46 22.60 25.85 27.36	5.004 5.024 5.011 5.014 5.007 5.004 5.998 6.004	0.264 0.474 0.761 1.014 2.007 3.004 3.988 4.504	1.64 1.73 1.90 2.04 2.49 2.78 2.92 3.09

	Series no. 3-8												
	$P_{atm} = 1.00 \text{ bar}$												
Set	T _G						Activa	ted line	es				
no.	(°Č)	B2 B3 B5											
		Fr _{L,B2}	P _{TC} (bar)	ΔP (bar)	$\frac{h_{OGE,B2}}{d}$	Fr _{L,B3}	P _{TC} (bar)	ΔP (bar)	$\frac{h_{OGE,B3}}{d}$	Fr _{L,B5}	P _{TC} (bar)	ΔP (bar)	$\frac{h_{OGE,B5}}{d}$
3-8.1 3-8.2 3-8.3 3-8.4 3-8.5 3-8.6 3-8.7 3-8.8	24.5 28.0 24.3 28.0 30.5 28.5 25.0 27.0	6.37 9.56 11.19 12.90 18.39 22.63 25.90 27.35	4.997 5.048 5.005 4.997 4.989 5.010 6.002 6.002	0.237 0.568 0.745 1.007 1.989 3.010 4.002 4.502	1.38 1.80 1.83 1.89 2.28 2.60 2.74 2.91	6.57 9.05 11.14 12.90 18.44 22.62 25.91 27.36	5.004 4.999 4.997 5.017 5.002 5.007 6.006 6.007	0.254 0.499 0.737 1.007 2.002 3.007 4.006 4.507	1.06 1.34 1.56 1.67 2.01 2.26 2.37 2.57	6.60 8.75 11.20 12.96 18.30 22.37 25.86 27.37	5.007 4.989 4.996 5.017 5.017 5.003 6.003 6.001	0.257 0.459 0.746 1.017 1.967 2.953 3.993 4.511	1.21 1.38 1.58 1.81 2.07 2.27 2.41 2.50

	Series no. 3-9												
						Pa	$_{\rm tm} = 1.0$	00 bar					
Set	TG						Activa	ted line	es				
no.	(°C)]	B2]	34]	B5	
		Fr _{L,B2}	P _{TC} (bar)	ΔP (bar)	$\frac{h_{OGE,B2}}{d}$	Fr _{L,B4}	P _{TC} (bar)	ΔP (bar)	$\frac{h_{OGE,B4}}{d}$	Fr _{L,B5}	P _{TC} (bar)	ΔP (bar)	$\frac{h_{OGE,B5}}{d}$
3-9.1 3-9.2 3-9.3 3-9.4 3-9.5 3-9.6 3-9.7 3-9.8	20.5 29.5 22.5 31.0 30.0 31.0 25.5 27.0	6.48 9.12 11.29 12.95 18.52 22.61 25.94 27.37	4.997 5.018 5.009 5.004 5.000 5.001 6.013 6.010	0.247 0.508 0.759 1.014 2.020 3.001 4.013 4.510	1.46 1.58 1.86 1.83 2.11 2.37 2.48 2.60	6.50 9.10 11.24 12.99 18.38 22.61 25.92 27.42	4.999 4.995 4.993 5.030 4.987 5.002 5.999 6.006	0.249 0.505 0.753 1.020 1.987 3.002 4.009 4.526	1.45 1.59 1.62 1.67 1.87 2.01 2.07 2.12	6.73 9.59 11.33 13.06 18.61 22.61 25.87 27.28	5.009 4.992 5.006 5.011 5.022 5.002 6.014 5.999	0.269 0.572 0.766 1.031 2.042 3.002 3.994 4.479	1.18 1.44 1.49 1.81 2.07 2.30 2.38 2.53

	Series no. 3-10												
						Pat	m = 1.0	0 bar					
Set	TG						Activa	ted line	es				
no.	(°Č)]	B3]	B4]	B5	
		Fr _{L,B3}	P _{TC} (bar)	ΔP (bar)	h _{OGE,B3} d	Fr _{L,B4}	P _{TC} (bar)	ΔP (bar)	$\frac{h_{OGE,B4}}{d}$	Fr _{L,B5}	P _{TC} (bar)	ΔP (bar)	h _{OGE,B5} d
3-10.1 3-10.2 3-10.3 3-10.4 3-10.5 3-10.6 3-10.7 3-10.8	25.0 28.5 23.5 31.5 30.5 31.3 25.0 27.0	6.49 9.08 11.24 12.85 18.55 22.61 25.78 27.37	4.997 4.983 5.002 5.007 4.998 5.001 5.990 6.000	0.247 0.503 0.752 0.997 2.028 3.001 3.970 4.510	1.11 1.37 1.56 1.76 2.09 2.37 2.52 2.68	6.57 9.47 11.11 12.96 18.50 22.51 25.87 27.31	5.004 5.056 4.993 5.015 5.006 5.000 5.994 5.989	0.254 0.556 0.733 1.015 2.016 2.980 3.994 4.489	1.34 1.56 1.67 1.76 2.01 2.29 2.43 2.58	6.48 9.35 11.22 12.91 18.37 22.62 25.89 27.35	4.996 5.009 4.999 5.016 5.015 5.003 6.010 6.004	$\begin{array}{c} 0.246\\ 0.539\\ 0.749\\ 1.006\\ 1.985\\ 3.003\\ 4.000\\ 4.504 \end{array}$	1.18 1.44 1.55 1.81 2.01 2.21 2.36 2.50

Table C.4 : Experimental	data for quadr	uple discharge
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	Series no. 4-1																
	$P_{atm} = 1.00 \text{ bar}$																
Set	T _G								Activat	ed lines							
no.	(°Č)		B1 B2 B3 B4														
		Fr _{L,B1}	P _{TC} (bar)	ΔP (bar)	$\frac{h_{OGE,B1}}{d}$	Fr _{L,B2}	P _{TC} (bar)	ΔP (bar)	$\frac{h_{OGE,B2}}{d}$	Fr _{L,B3}	P _{TC} (bar)	ΔP (bar)	$\frac{h_{OGE,B3}}{d}$	Fr _{L,B4}	P _{TC} (bar)	ΔP (bar)	$\frac{h_{OGE,B4}}{d}$
4-1.1 4-1.2 4-1.3 4-1.4 4-1.5 4-1.6 4-1.7 4-1.8	29.0 36.0 25.5 32.0 27.0 28.6 22.5 27.5	6.52 9.08 11.27 12.78 18.45 22.53 25.89 27.36	4.999 5.000 4.995 4.975 5.009 5.009 5.994 6.007	0.249 0.500 0.755 0.985 2.009 2.989 4.004 4.507	1.38 1.64 1.87 1.79 2.25 2.65 2.68 2.91	6.52 9.00 11.23 12.84 18.48 22.61 25.85 27.43	4.999 4.990 5.000 4.995 5.016 5.005 5.992 5.998	0.249 0.490 0.750 0.995 2.016 3.005 3.992 4.528	1.46 1.49 1.69 1.86 2.37 2.65 2.85 3.05	6.43 9.24 11.30 12.86 18.37 22.62 25.84 27.36	5.001 5.012 5.000 4.998 4.990 5.007 5.990 6.005	0.254 0.496 0.751 0.982 2.017 3.002 4.010 4.493	$ \begin{array}{c} 1.25\\ 1.56\\ 1.70\\ 1.95\\ 2.37\\ 2.71\\ 3.00\\ 3.11 \end{array} $	6.51 9.09 11.23 12.86 18.48 22.61 25.85 27.43	4.998 5.012 5.000 4.999 5.014 5.005 5.992 5.998	0.247 0.494 0.763 0.963 2.041 3.008 4.001 4.498	1.59 1.67 1.90 2.04 2.52 2.89 3.09 3.26

Table C.4 : Experimental data for quadruple discharge (cont.)

	Series no. 4-2																
	$P_{atm} = 1.00 \text{ bar}$																
Set	TG								Activate	ed lines							
no.	(°Ĉ)			B1		B2 B3 B5											
		Fr _{L,B1}	P _{TC} (bar)	ΔP (bar)	h _{OGE,B1} d	Fr _{L,B2}	P _{TC} (bar)	ΔP (bar)	$\frac{h_{OGE,B2}}{d}$	Fr _{L,B3}	P _{TC} (bar)	ΔP (bar)	$\frac{h_{OGE,B3}}{d}$	Fr _{L,B5}	P _{TC} (bar)	ΔP (bar)	h _{OGE,B5} d
4-2.1 4-2.2 4-2.3 4-2.4 4-2.5 4-2.6 4-2.7 4-2.8	29.0 36.0 25.5 32.0 28.0 28.8 23.0 27.5	6.57 9.05 11.24 12.76 18.49 22.60 25.91 27.32	5.004 4.996 5.001 5.002 5.017 5.002 6.010 6.003	0.254 0.496 0.751 0.982 2.017 3.002 4.010 4.493	1.38 1.59 1.76 1.99 2.25 2.45 2.65 2.79	6.62 9.26 11.20 12.88 18.41 22.61 25.82 27.31	4.997 5.004 5.003 4.993 5.051 4.998 6.001 5.998	0.247 0.494 0.763 0.963 2.041 3.008 4.001 4.498	$1.24 \\ 1.35 \\ 1.46 \\ 1.58 \\ 2.03 \\ 2.34 \\ 2.42 \\ 2.60$	6.62 9.26 11.20 12.88 18.41 22.61 25.82 27.31	5.008 5.024 4.995 5.002 5.008 5.006 5.995 5.989	0.258 0.524 0.745 1.002 1.998 3.006 3.985 4.489	1.11 1.34 1.50 1.67 2.01 2.23 2.37 2.54	6.55 9.05 11.24 12.78 18.45 22.60 25.84 27.33	5.002 4.996 5.001 5.006 5.008 5.002 6.001 6.004	0.252 0.496 0.751 0.986 2.008 3.002 3.991 4.494	1.32 1.49 1.78 1.92 2.18 2.44 2.64 2.85

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Table C.4 : Experimental	data for quadr	uple discharge	(cont.)
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	Series no. 4-3 P _{atm} = 1.00 bar																
Set	Set T _G Activated lines																
no.	(°C)	B1 B2 B4 B5															
		Fr _{L,B1}	P _{TC} (bar)	ΔP (bar)	$\frac{h_{OGE,B1}}{d}$	Fr _{L,B2}	P _{TC} (bar)	ΔP (bar)	$\frac{h_{OGE,B2}}{d}$	Fr _{L,B4}	P _{TC} (bar)	ΔP (bar)	$\frac{h_{OGE,B4}}{d}$	Fr _{L,B5}	P _{TC} (bar)	ΔP (bar)	$\frac{h_{OGE,B5}}{d}$
4-3.1 4-3.2 4-3.3 4-3.4 4-3.5 4-3.6 4-3.7 4-3.8	29.0 36.0 26.0 35.0 35.0 29.0 23.5 28.0	6.62 9.11 11.33 12.75 18.43 22.62 25.90 27.34	5.008 5.005 5.004 4.999 5.003 5.007 6.007 5.996	0.258 0.505 0.764 0.979 1.993 3.007 4.007 4.496	$1.21 \\ 1.41 \\ 1.81 \\ 1.64 \\ 2.13 \\ 2.45 \\ 2.65 \\ 2.79$	6.48 9.08 11.23 12.96 18.40 22.56 25.87 27.29	4.996 4.991 5.000 5.042 4.985 4.993 5.996 5.991	0.246 0.501 0.750 1.012 1.985 2.993 3.996 4.481	1.13 1.21 1.46 1.49 1.83 2.06 2.25 2.45	6.51 9.08 11.28 13.14 18.38 22.55 25.90 27.25	4.998 5.000 5.007 5.042 4.981 4.991 5.995 5.988	0.248 0.500 0.757 1.042 1.981 2.991 4.005 4.468	1.22 1.48 1.53 1.62 1.81 2.07 2.10 2.24	6.52 9.32 11.22 12.75 18.44 22.56 25.94 27.42	5.009 5.012 5.008 4.999 5.005 5.015 6.006 6.015	0.249 0.532 0.748 0.979 1.995 2.995 4.016 4.525	1.21 1.46 1.66 1.61 2.21 2.50 2.73 2.79

Table C.4 : Experimental	data for quadru	ple discharge	(cont.)
1	1		` /

	Series no. 4-4 $P_{atm} = 1.00 \text{ bar}$																
Set T _c Activated lines																	
no.	(°C)	C) B1 B3]	B4		B5				
		Fr _{L,B1}	P _{TC} (bar)	ΔP (bar)	$\frac{h_{OGE,B1}}{d}$	Fr _{L,B3}	P _{TC} (bar)	ΔP (bar)	$\frac{h_{OGE,B3}}{d}$	Fr _{L,B4}	P _{TC} (bar)	ΔP (bar)	$\frac{h_{OGE,B4}}{d}$	Fr _{L,B5}	P _{TC} (bar)	ΔP (bar)	$\frac{h_{OGE,B5}}{d}$
4-4.1 4-4.2 4-4.3 4-4.4 4-4.5 4-4.6 4-4.7 4-4.8	29.0 36.0 26.0 32.0 34.5 29.3 24.0 27.5	6.59 9.27 11.27 12.89 18.48 22.58 25.93 27.38	5.005 5.026 5.006 5.004 5.025 5.008 6.013 6.003	0.255 0.526 0.756 1.004 2.005 2.998 4.013 4.513	1.30 1.47 1.76 1.96 2.22 2.33 2.56 2.59	6.64 9.24 11.29 12.81 18.41 22.59 25.88 27.31	5.000 5.012 5.009 4.991 4.990 5.000 5.998 5.990	0.260 0.522 0.759 0.991 1.990 3.000 3.998 4.490	1.14 1.39 1.53 1.73 2.09 2.35 2.52 2.66	6.51 9.17 11.22 12.71 18.47 22.76 25.89 27.29	4.998 5.002 4.998 4.995 5.003 5.016 6.002 5.982	0.248 0.512 0.748 0.975 2.003 3.036 4.002 4.482	$ \begin{array}{r} 1.36\\ 1.48\\ 1.59\\ 1.70\\ 2.04\\ 2.35\\ 2.46\\ 2.58\\ \end{array} $	6.54 9.31 11.28 12.94 18.48 22.68 25.84 27.35	5.001 5.021 5.007 5.011 5.025 5.019 5.999 6.003	0.251 0.531 0.757 1.011 2.005 3.019 3.989 4.503	1.29 1.46 1.78 1.98 2.33 2.41 2.64 2.73

Table C.4 : Experimental data for quadruple discharge (cont.)

	Series no. 4-5																
	$P_{atm} = 1.00 \text{ bar}$																
Set T _G Activated lines																	
no.	(°C)	B2 B3								B4				B5			
		Fr _{L,B2}	P _{TC} (bar)	ΔP (bar)	$\frac{h_{OGE,B2}}{d}$	Fr _{L,B3}	P _{TC} (bar)	ΔP (bar)	$\frac{h_{OGE,B3}}{d}$	Fr _{L,B4}	P _{TC} (bar)	ΔP (bar)	$\frac{h_{OGE,B4}}{d}$	Fr _{L,B5}	P _{TC} (bar)	ΔP (bar)	$\frac{h_{OGE,B5}}{d}$
4-5.1 4-5.2 4-5.3 4-5.4 4-5.5 4-5.6 4-5.7 4-5.8	28.0 37.0 26.0 32.0 27.5 29.2 24.5 27.5	6.57 9.08 11.23 12.57 18.45 22.55 25.84 27.40	5.004 5.010 4.999 4.981 4.998 5.001 6.007 6.009	0.254 0.500 0.749 0.951 2.008 2.991 3.987 4.519	1.69 1.77 1.94 2.06 2.60 2.79 3.14 3.31	6.66 9.01 11.21 12.76 18.49 22.66 25.97 27.45	5.002 5.001 4.997 4.982 5.007 5.015 6.005 6.005	0.262 0.491 0.747 0.982 2.017 3.015 4.025 4.535	1.23 1.56 1.73 1.95 2.43 2.74 3.02 3.14	6.35 9.09 11.21 12.71 18.55 22.54 25.91 27.25	4.994 5.001 4.996 4.975 5.011 5.000 6.008 5.970	0.234 0.501 0.746 0.975 2.031 2.990 4.008 4.470	1.45 1.56 1.73 1.84 2.24 2.52 2.72 2.83	6.62 9.19 11.26 12.58 18.48 22.69 25.89 27.26	5.008 5.005 5.004 4.984 5.025 5.031 6.011 5.993	0.258 0.515 0.754 0.954 2.015 3.021 4.001 4.473	1.26 1.58 1.72 1.72 2.18 2.47 2.62 2.73

	Series no. 5-1													
	$P_{atm} = 1.00 \text{ bar}$													
Set	Set T _G Activated lines													
no.	(°Č)]	B1	-]	B2	-	B3				
		Fr _{L,B1}	P _{TC} (bar)	ΔP (bar)	$\frac{h_{OGE,B1}}{d}$	Fr _{L,B2}	P _{TC} (bar)	ΔP (bar)	$\frac{h_{OGE,B2}}{d}$	Fr _{L,B3}	P _{TC} (bar)	ΔP (bar)	$\frac{h_{OGE,B3}}{d}$	
5-1.1 5-1.2 5-1.3 5-1.4 5-1.5 5-1.6 5-1.7 5-1.8	27.5 35.5 24.8 32.0 27.0 30.0 25.0 27.5	6.47 9.08 11.24 12.85 18.34 22.50 25.87 27.28	4.995 5.001 5.002 4.977 5.002 5.030 6.014 5.998	0.245 0.501 0.752 0.997 1.982 2.980 3.994 4.478	1.41 1.79 1.87 2.04 2.33 2.53 2.77 2.85	6.49 9.09 11.15 13.08 18.29 22.34 25.73 27.07	4.997 5.002 4.998 5.003 5.000 4.945 5.996 6.009	0.247 0.502 0.738 1.033 1.970 2.945 3.956 4.409	1.41 1.46 1.69 1.92 2.37 2.65 2.91 3.05	6.62 9.07 11.24 12.88 18.67 22.72 25.87 27.23	5.008 4.999 5.002 5.002 5.030 5.027 5.986 5.992	0.258 0.499 0.752 1.002 2.060 3.027 3.996 4.462	1.28 1.48 1.70 1.95 2.37 2.80 2.97 3.14	

	Series no. 5-1 (cont.)													
	P _{atm} = 1.00 bar													
Set	Set T _G Activated lines													
no.	(°Č)		B4 B5											
		Fr _{L,B4}	P _{TC} (bar)	ΔP (bar)	$\frac{h_{OGE,B4}}{d}$	Fr _{L,B5}	P _{TC} (bar)	ΔP (bar)	$\frac{h_{OGE,B5}}{d}$					
5-1.1 5-1.2 5-1.3 5-1.4 5-1.5 5-1.6 5-1.7 5-1.8	27.5 35.5 24.8 32.0 27.0 30.0 25.0 27.5	6.62 9.04 11.22 13.08 18.35 22.87 25.89 27.11	4.998 4.995 4.999 5.003 4.994 5.058 6.001 6.003	0.258 0.495 0.749 1.033 1.984 3.058 4.001 4.423	1.42 1.50 1.73 1.84 2.26 2.60 2.75 2.86	6.67 9.13 11.24 12.85 18.42 22.27 25.79 27.28	5.003 5.007 5.002 4.977 4.992 5.000 6.003 5.998	0.263 0.507 0.752 0.997 2.002 2.930 3.973 4.478	1.46 1.69 1.75 1.98 2.27 2.50 2.88 2.96					

Table C.5 : Experimental data for quintuple discharge (cont.)

Appendix D

Images of Typical Gas Entrainment Phenomena for Dual, Triple, and Quadruple Discharge Conditions



(c) Disappearance of unsteady flow at B1

(d) Steady flow at B1

Figure D.1 : Gas entrainment phenomena of set no. 2-1.1



(g) Disappearance of unsteady flow at B2

(h) Steady flow at B2

Figure D.1 : Gas entrainment phenomena of set no. 2-1.1 (cont.)



Figure D.2 : Gas entrainment phenomena of set no. 2-2.1



Figure D.2 : Gas entrainment phenomena of set no. 2-2.1 (cont.)



- (c) Disappearance of unsteady flow at B1
- (d) Steady flow at B1

Figure D.3 : Gas entrainment phenomena of set no. 2-3.1



- (g) Disappearance of unsteady flow at B4
- (h) Steady flow at B4

Figure D.3 : Gas entrainment phenomena of set no. 2-3.1 (cont.)



Figure D.4 : Gas entrainment phenomena of set no. 2-4.1







Figure D.4 : Gas entrainment phenomena of set no. 2-4.1 (cont.)



Figure D.5 : Gas entrainment phenomena of set no. 2-5.1



Figure D.5 : Gas entrainment phenomena of set no. 2-5.1 (cont.)



(c) Disappearance of unsteady flow at B2

(d) Steady flow at B2

Figure D.6 : Gas entrainment phenomena of set no. 2-6.1



- (g) Disappearance of unsteady flow at B4
- (h) Steady flow at B4

Figure D.6 : Gas entrainment phenomena of set no. 2-6.1 (cont.)



- (c) Disappearance of unsteady flow at B2
- (d) Steady flow at B2

Figure D.7 : Gas entrainment phenomena of set no. 2-7.1



Figure D.7 : Gas entrainment phenomena of set no. 2-7.1 (cont.)



Figure D.8 : Gas entrainment phenomena of set no. 2-8.1







Figure D.9 : Gas entrainment phenomena of set no. 2-9.1



Figure D.9 : Gas entrainment phenomena of set no. 2-9.1 (cont.)



- (c) Disappearance of unsteady flow at B4
- (d) Steady flow at B4

Figure D.10 : Gas entrainment phenomena of set no. 2-10.1







Figure D.10 : Gas entrainment phenomena of set no. 2-10.1 (cont.)



Initial depression at B1 (a)



Unsteady flow at B1 (b)



Disappearance of unsteady flow at B1 (c)



(d) Steady flow at B1



Initial depression at B2 (e)

B

OFTESTALECE

Unsteady flow at B2 (f)

Figure D.11 : Gas entrainment phenomena of set no. 3-1.1

B2



(k) Disappearance of unsteady flow at B3

(l) Steady flow at B3

Figure D.11 : Gas entrainment phenomena of set no. 3-1.1 (cont.)


(c) Disappearance of unsteady flow at B1



3013-02-03 02:23:55

B1



(e) Initial depression at B2

B4

CINTEST RECE

(f) Unsteady flow at B2



2013-02-03 02:24:07

B1

B2



Disappearance of unsteady flow at B4

Steady flow at B4 (l)

Figure D.12 : Gas entrainment phenomena of set no. 3-2.1 (cont.)



Figure D.13 : Gas entrainment phenomena of set no. 3-3.1



Figure D.13 : Gas entrainment phenomena of set no. 3-3.1 (cont.)



Initial depression at B1 (a)



Unsteady flow at B1 (b)

2013-02-03 10/22:47

B1

2013-02-03 10:23:45



(c)



Initial depression at B3 (e)

ONTESTRECE B4

B1 CHIESTREE B4 **B**3

B3



Figure D.14 : Gas entrainment phenomena of set no. 3-4.1



- (k) Disappearance of unsteady flow at B4
- (l) Steady flow at B4

Figure D.14 : Gas entrainment phenomena of set no. 3-4.1 (cont.)



Figure D.15 : Gas entrainment phenomena of set no. 3-5.1



Figure D.15 : Gas entrainment phenomena of set no. 3-5.1 (cont.)



Figure D.16 : Gas entrainment phenomena of set no. 3-6.1



Figure D.16 : Gas entrainment phenomena of set no. 3-6.1 (cont.)



(a) Initial depression at B2



(b) Unsteady flow at B2 and Initial depression at B4



Figure D.17 : Gas entrainment phenomena of set no. 3-7.1





(h) Steady flow at B3



(i) Unsteady flow at B4



(j) Disappearance of unsteady flow at B4



(k) Steady flow at B4

Figure D.17 : Gas entrainment phenomena of set no. 3-7.1 (cont.)



(b) Unsteady flow at B2



(c) Disappearance of unsteady flow at B2



(d) Steady flow at B2

2013-02-03 12:12:07



- (e) Initial depression at B3
- B5 SPTESTREE B3 B2
 - (f) Unsteady flow at B3
- Figure D.18 : Gas entrainment phenomena of set no. 3-8.1





(h) Steady flow at B3



(i) Initial depression at B5



(j) Unsteady flow at B5



(k) Disappearance of unsteady flow at B5



(l) Steady flow at B5





Figure D.19 : Gas entrainment phenomena of set no. 3-9.1



- (k) Disappearance of unsteady flow at B5
- (l) Steady flow at B5







(b) Unsteady flow at B3

2013-02-03 12-53-55



(c) Disappearance of unsteady flow at B3



B5



(e) Initial depression at B4

(f) Unsteady flow at B4





2013-02-02 12:50:45

(k) Disappearance of unsteady flow at B5



2013-02-03 12:50:53

Figure D.20 : Gas entrainment phenomena of set no. 3-10.1 (cont.)



(a) Initial depression at B1



(b) Unsteady flow at B1



(c) Disappearance of unsteady flow at B1



(e) Initial depression at B2



(d) Steady flow at B1





Figure D.21 : Gas entrainment phenomena of set no. 4-1.1



Disappearance of unsteady flow at B3

(1) Steady flow at B3

Figure D.21 : Gas entrainment phenomena of set no. 4-1.1 (cont.)



(o) Disappearance of unsteady flow at B4

(p) Steady flow at B4

Figure D.21 : Gas entrainment phenomena of set no. 4-1.1 (cont.)



Figure D.22 : Gas entrainment phenomena of set no. 4-2.1



Figure D.22 : Gas entrainment phenomena of set no. 4-2.1 (cont.)





(o) Steady flow at B5

Figure D.22 : Gas entrainment phenomena of set no. 4-2.1 (cont.)



Figure D.23 : Gas entrainment phenomena of set no. 4-3.1



Figure D.23 : Gas entrainment phenomena of set no. 4-3.1 (cont.)



(a) Initial depression at B1



(b) Unsteady flow at B1 and Initial depression at B5



Figure D.24 : Gas entrainment phenomena of set no. 4-4.1



(k) Disappearance of unsteady flow at B4









(o) Steady flow at B5

Figure D.24 : Gas entrainment phenomena of set no. 4-4.1 (cont.)





(e) Initial depression at B3

- (f) Unsteady flow at B3
- Figure D.25 : Gas entrainment phenomena of set no. 4-5.1



(k) Disappearance of unsteady flow at B4



Figure D.25 : Gas entrainment phenomena of set no. 4-5.1 (cont.)



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(o) Disappearance of unsteady flow at B5



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Figure D.25 : Gas entrainment phenomena of set no. 4-5.1 (cont.)